



Instruction Manual

Model

720A

Kelvin-Varley
Voltage Divider

P/N 294058

MARCH, 1969

Rev. 2 9/20/74

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2. On receipt of the shipping instructions, forward the instrument, transportation prepaid. Repairs will be made at the Service Facility and the instrument returned, transportation prepaid.

SHIPPING TO MANUFACTURER FOR REPAIR OR ADJUSTMENT

All shipments of John Fluke Mfg. Co., Inc., instruments should be made via United Parcel Service or "Best Way*" prepaid. The instrument should be shipped in the original packing carton; or if it is not available, use any suitable container that is rigid and of adequate size. If a substitute container is used, the instrument should be wrapped in paper and surrounded with at least four inches of excelsior or similar shock-absorbing material.

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The instrument should be thoroughly inspected immediately upon original delivery to purchaser. All material in the container should be checked against the enclosed packing list. The manufacturer will not be responsible for shortages against the packing sheet unless notified immediately. If the instrument is damaged in any way, a claim should be filed with the carrier immediately. (To obtain a quotation to repair shipment damage, contact the nearest Fluke Technical Center.) Final claim and negotiations with the carrier must be completed by the customer.

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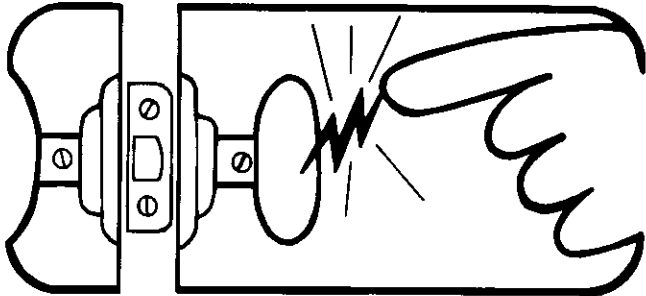
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static awareness



A Message From
John Fluke Mfg. Co., Inc.

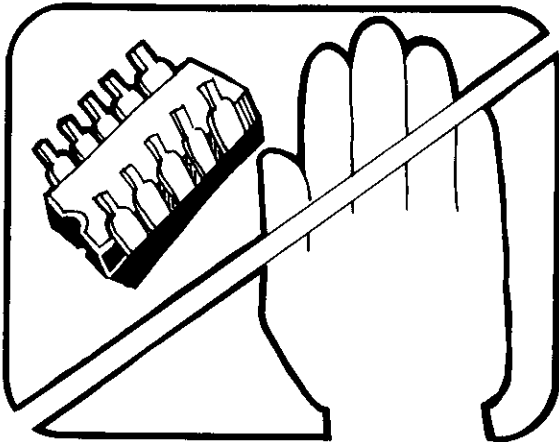


Some semiconductors and custom IC's can be damaged by electrostatic discharge during handling. This notice explains how you can minimize the chances of destroying such devices by:

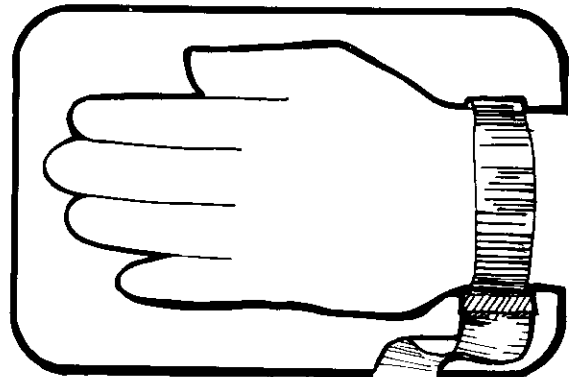
1. Knowing that there is a problem.
2. Learning the guidelines for handling them.
3. Using the procedures, and packaging and bench techniques that are recommended.

The Static Sensitive (S.S.) devices are identified in the Fluke technical manual parts list with the symbol "⊗".

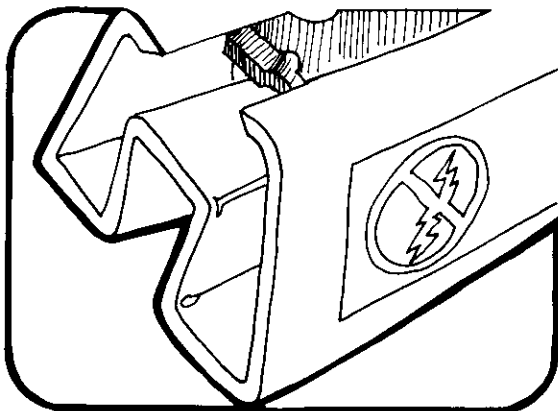
The following practices should be followed to minimize damage to S.S. devices.



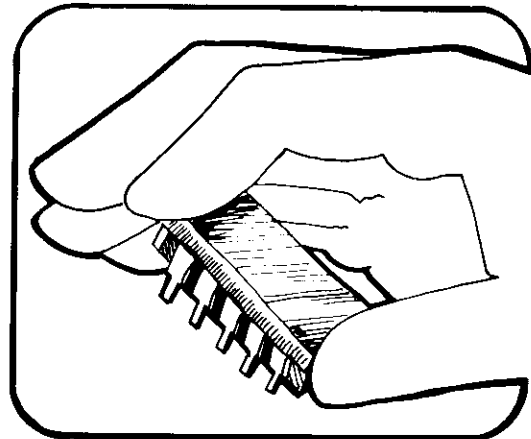
1. MINIMIZE HANDLING



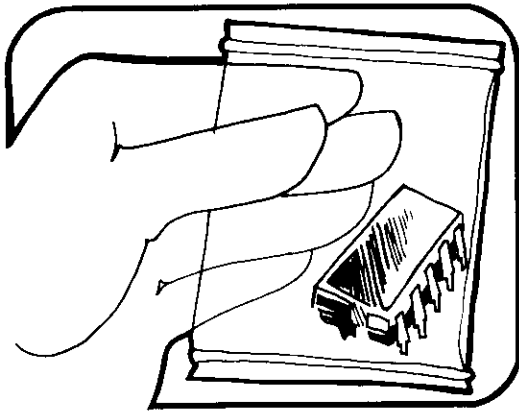
3. DISCHARGE PERSONAL STATIC BEFORE HANDLING DEVICES



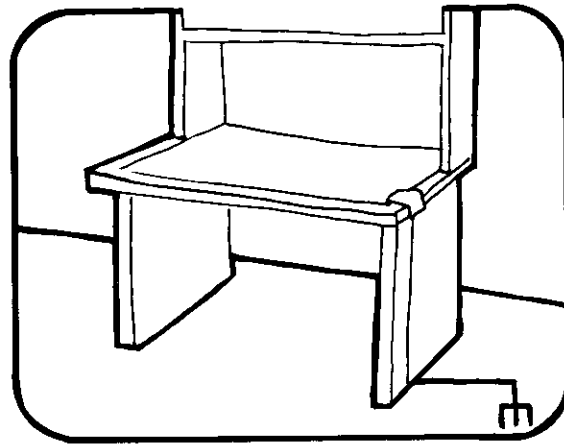
2. KEEP PARTS IN ORIGINAL CONTAINERS UNTIL READY FOR USE.



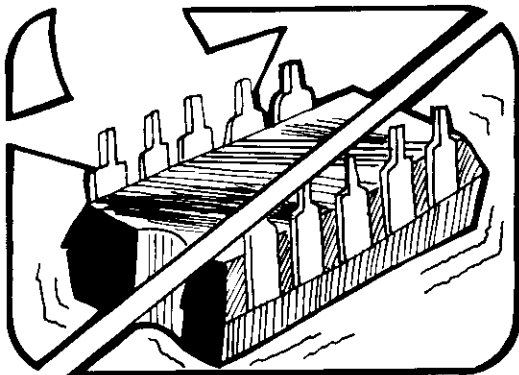
4. HANDLE S.S. DEVICES BY THE BODY



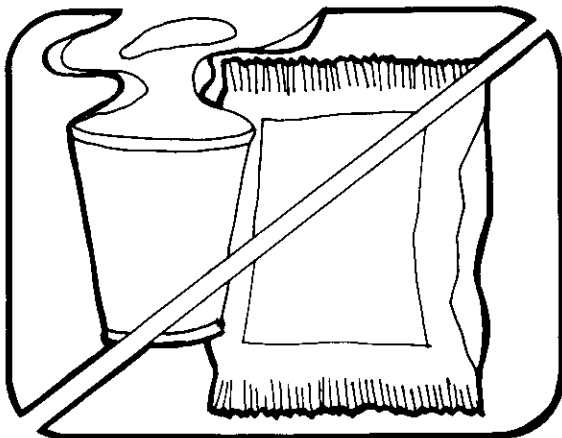
5. USE ANTI-STATIC CONTAINERS FOR HANDLING AND TRANSPORT



8. HANDLE S.S. DEVICES ONLY AT A STATIC-FREE WORK STATION
9. ONLY ANTI-STATIC TYPE SOLDER-SUCKERS SHOULD BE USED.
10. ONLY GROUNDED TIP SOLDERING IRONS SHOULD BE USED.



6. DO NOT SLIDE S.S. DEVICES OVER ANY SURFACE



7. AVOID PLASTIC, VINYL AND STYROFOAM IN WORK AREA

Anti-static bags, for storing S.S. devices or pcbs with these devices on them, can be ordered from the John Fluke Mfg. Co., Inc.. See section 5 in any Fluke technical manual for ordering instructions. Use the following part numbers when ordering these special bags.

John Fluke Part No.	Bag Size
453522	6" x 8"
453530	8" x 12"
453548	16" x 24"
454025	12" x 15"

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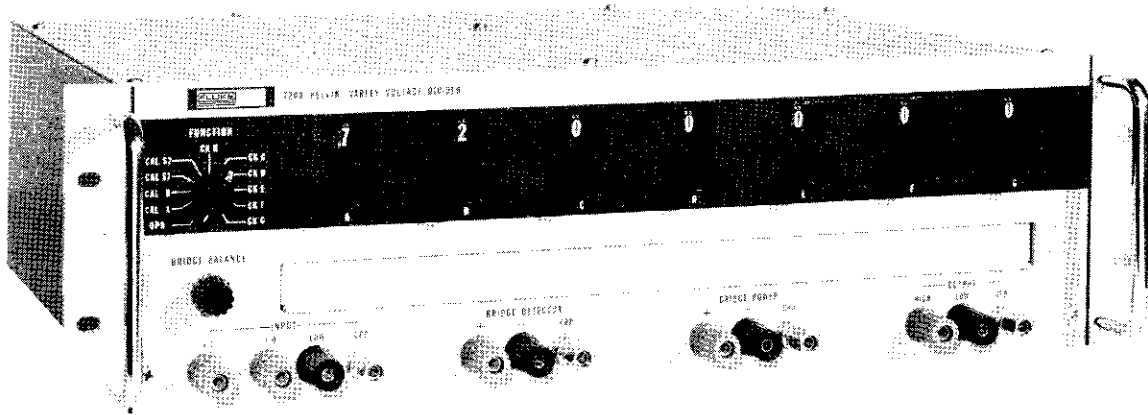
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MODEL 720A KELVIN-VARLEY VOLTAGE DIVIDER

Section 1

Introduction & Specifications

1-1. INTRODUCTION

1-2. The Model 720A Kelvin-Varley Voltage Divider is a seven-dial primary ratio standard which meets the most exacting requirements of the standards laboratory. Absolute linearity of 0.1 ppm, temperature coefficient of linearity of 0.1 ppm/°C, and self-calibration make the 720A the most accurate instrument available for the comparison of primary and secondary voltage and resistance standards. The linearity has a small power derating coefficient of 0.2 ppm per watt which is achieved by matching the resistors' temperature coefficients close to zero. This permits operation at up to 1100 volts and 11 watts.

1-3. The Model 720A has two high input terminals. The terminal labeled INPUT 1.0 is for general use in all Kelvin-Varley applications for which direct reading, in ratio, is desired. The terminal labeled INPUT 1.1 is used for voltage measurement applications when both direct reading in voltage and over-ranging are desired. An example of this application is the measurement of standard cell voltages. Use of the 1.1 INPUT at a level of 1.1 volts in this application results in divider resolution of 0.1 microvolt and allows comparison of standard cells to within 1 microvolt.

1-4. Only thoroughly aged resistors of the highest quality are used in the Model 720A Kelvin-Varley Divider. As a result, linearity change per year will not exceed one part per million unless the instrument is subjected to abuse. To assure that the divider remains within its specifications throughout its useful life, adjustments are provided for the resistors of the first three decades. The third decade adjustments normally will be used only during annual calibration. Performing the self calibration procedure sets the adjustments of the first two decades. With reasonable care these adjustments will provide instrument accuracy of 0.1 part per million at the time of adjustment.

1-5. ELECTRICAL SPECIFICATIONS

RATIO RANGE

0 to 1.0 (1.0 INPUT TAP) and 0 to 1.1 (1.1 INPUT TAP).

RESOLUTION

0.1 ppm of input with 7 decades.

ABSOLUTE LINEARITY

(at calibration temperature and without the use of a correction chart)*

±0.1 ppm of input at dial settings of 1.1 to 0.1.

±0.1 (10S)^{1/3} of input at dial settings (S) of 0.1 to 0. (See Figure 1-1.)

ABSOLUTE LINEARITY STABILITY (without self-calibration)

±1.0 ppm of input/year at dial settings of 1.1 to 0.1.

±1.0 (10S)^{2/3} ppm of input/year at dial settings (S) of 0.1 to 0.

(See Figure 1-2.)

NOTE!

The self-calibration procedure may be used at any time to reset absolute linearity to ±0.1 ppm of input.

TEMPERATURE COEFFICIENT OF LINEARITY

±0.1 ppm of input/°C maximum at dial settings of 1.1 to 0.1.

(See Figure 1-3.)

SHORT-TERM LINEARITY STABILITY

Under typical conditions in a standards laboratory environment (temperature maintained within ±1°C) and with an applied voltage of up to 100 volts, stability of linearity is 0.1 ppm/30 days.

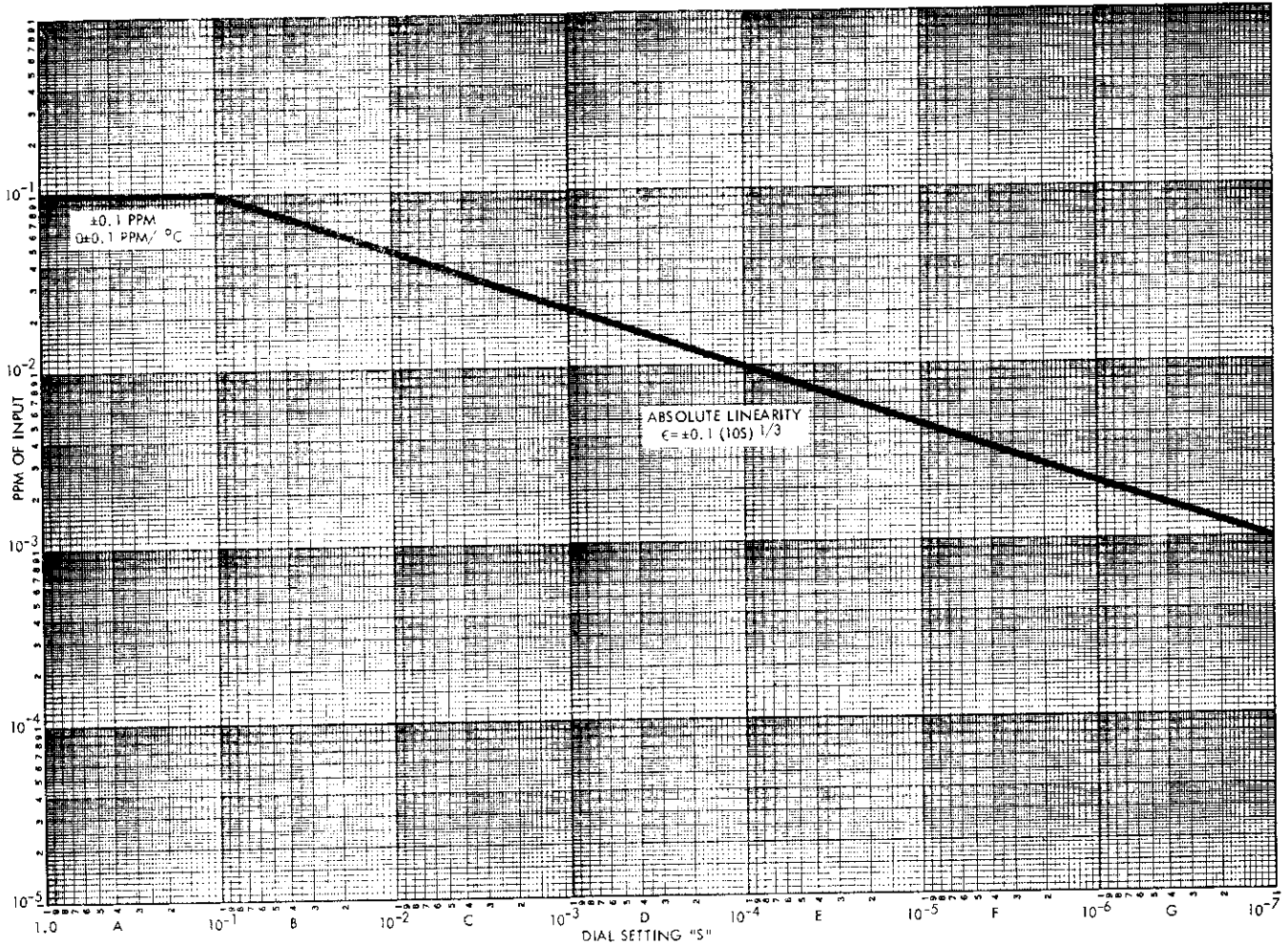


Figure 1-1. ABSOLUTE LINEARITY

POWER COEFFICIENT OF LINEARITY

± 0.2 ppm of input/watt maximum at dial settings of 1.1 to 0.1.

$\pm 0.2 (10S)^2$ ppm of input/watt maximum at dial settings (S) of 0.1 to 0.
(See Figure 1-4.)

MAXIMUM END ERRORS

Zero error, at output low	0.004 ppm of input
Zero error, at input low	0.05 ppm of input
Full-scale error	0.05 ppm of input

THERMAL VOLTAGES

± 0.5 uv maximum.

MAXIMUM INPUT POWER

10 watts on 1.0 INPUT terminal.
11 watts on 1.1 INPUT terminal.

*Absolute linearity is defined as the linearity between maximum and minimum output voltages.

MAXIMUM INPUT VOLTAGE

1000 volts on 1.0 INPUT terminal.
1100 volts on 1.1 INPUT terminal.

BREAKDOWN VOLTAGE

2000 volts to case at 10,000 feet.
2500 volts to case at sea level.

INPUT RESISTANCE

100 kilohms $\pm 0.005\%$ at 1.0 INPUT terminal at 25°C.
110 kilohms $\pm 0.005\%$ at 1.1 INPUT terminal at 25°C.

TEMPERATURE COEFFICIENT OF INPUT RESISTANCE

± 1 ppm/°C maximum.

MAXIMUM OUTPUT RESISTANCE

66 kilohms.

1-6. MECHANICAL AND ENVIRONMENTAL SPECIFICATIONS**OPERATING TEMPERATURE RANGE**

0°C to 50°C (32°F to 122°F).

NOTE!

When the Model 720A is used at temperatures below 15°C (59°F) or above 35°C (95°F), the range of the calibration adjustments may be

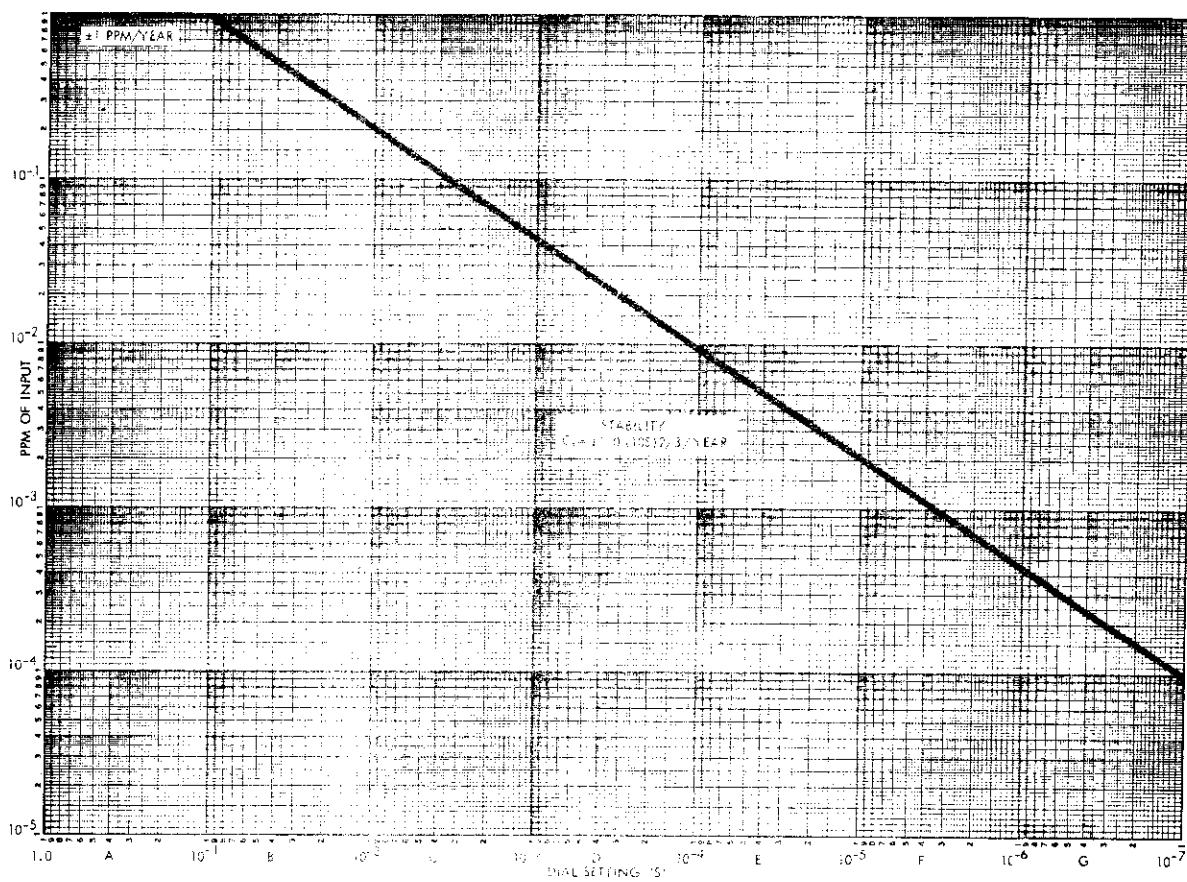


Figure 1-2. STABILITY

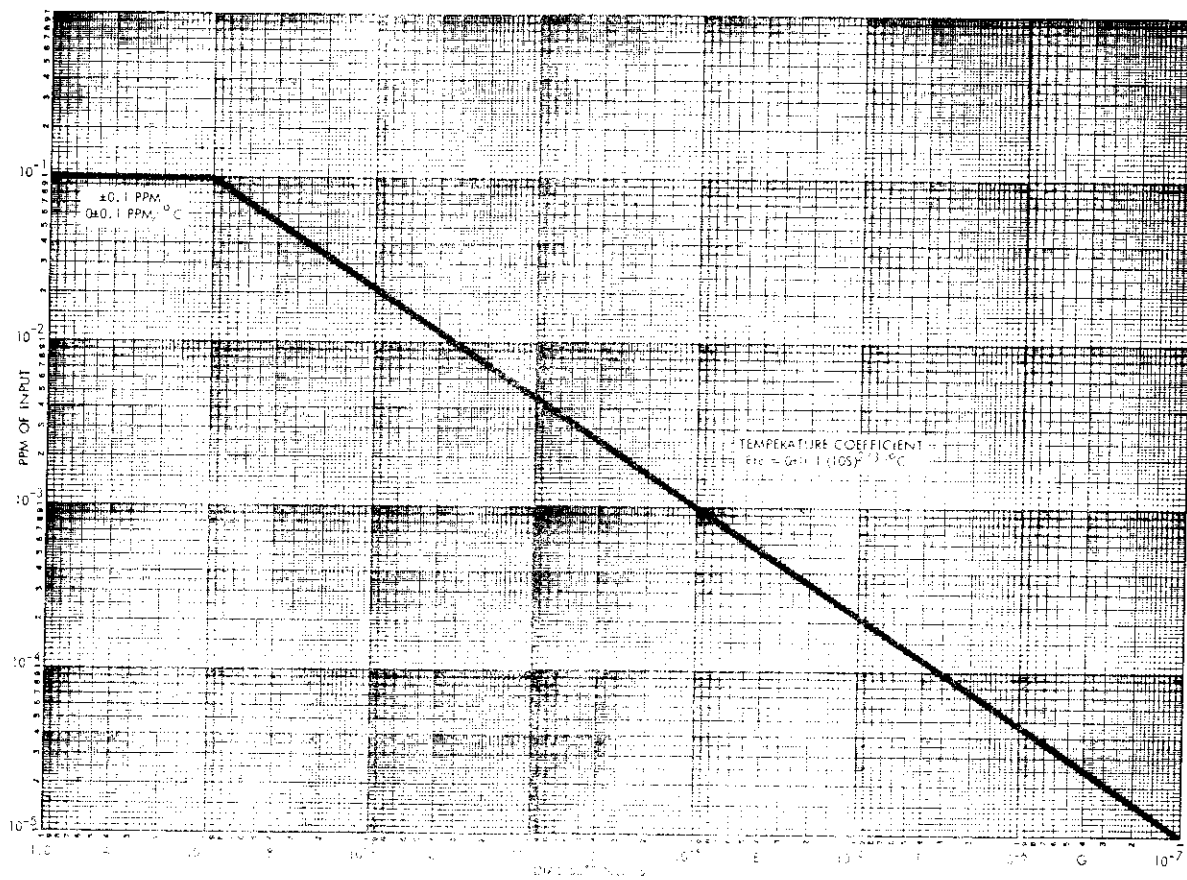


Figure 1-3. TEMPERATURE COEFFICIENT

exceeded and linearity must be derated 0.1 ppm/°C from the calibration temperature.

STORAGE TEMPERATURE RANGE
 -34°C to 70°C (-29°F to 158°F).

SHOCK

Meets requirements of MIL-T-945A and MIL-S-901B, rigidly mounted with slides.

VIBRATION

Meets requirements of MIL-T-945A, rigidly mounted or rack mounted with slides.

OPERATING HUMIDITY RANGE

Up to 70% relative humidity at 35°C (95°F): No derating is required.

Up to 80% relative humidity at 35°C (95°F): Linearity derating is 0.1 ppm of input for any relative humidity between 70% and 80%.

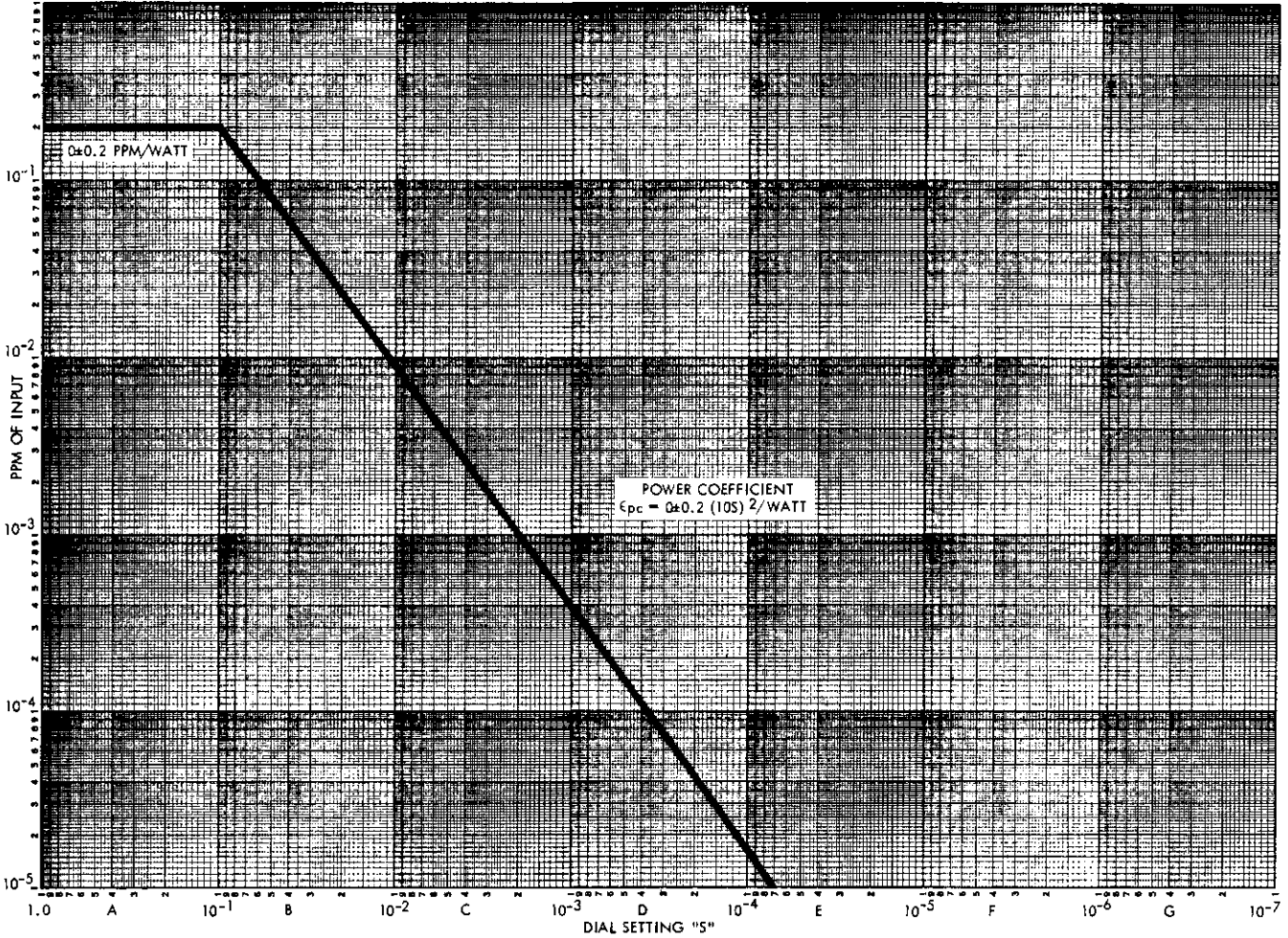


Figure 1-4. POWER COEFFICIENT

Section 2

Operating Instructions

2-1. INTRODUCTION

2-2. Although the Model 720A is a primary ratio standard it has the versatility necessary for use in a wide variety of measurement and control applications. In most applications the divider is used as an element of a system for measuring ratios, voltages, or resistances.

2-3. POWER LIMITATIONS

2-4. It is possible to damage the Model 720A by applying voltages incorrectly to the input terminals or by drawing more than 11 milliamperes from the output tap. The instrument will be damaged if a potential greater than 200 volts is applied between the 1.0 INPUT terminal and the 1.1 INPUT terminal. To prevent damage caused by drawing excessive current from the output tap, either the input or the output can be fused for 11 milliamperes. Another method of protecting the instrument is through the use of a power supply with current limiting capability. The current limit should be set for 11 milliamperes or less.

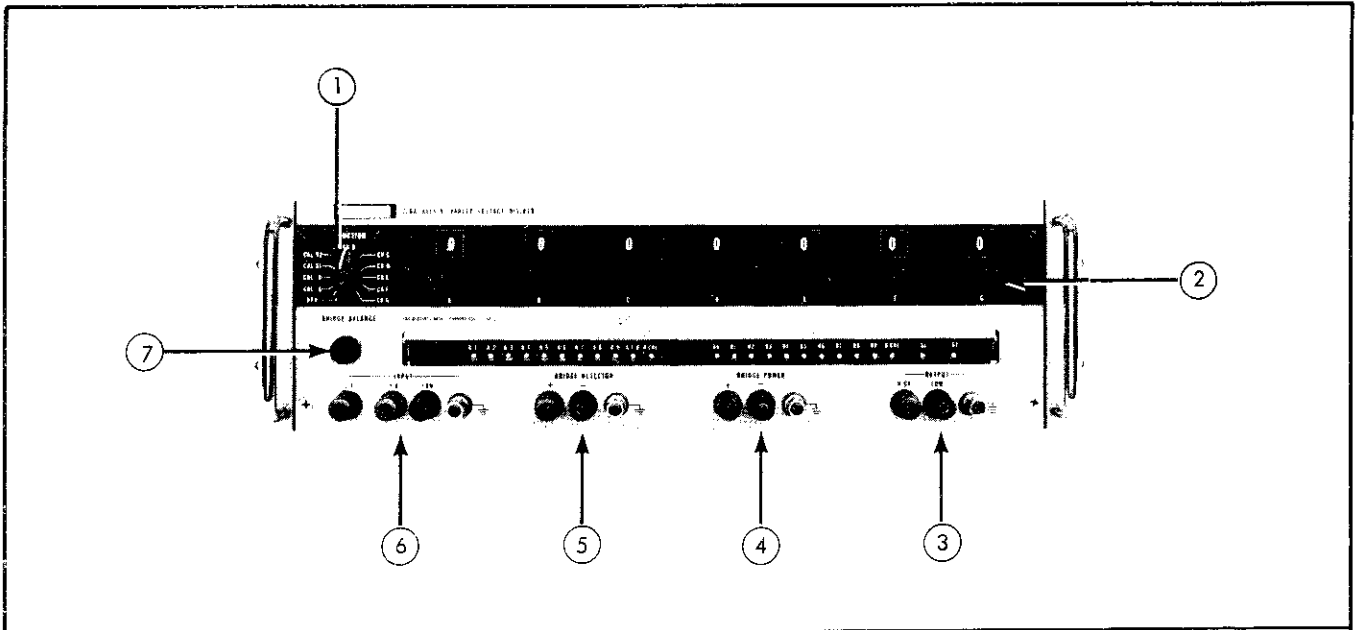
2-5. FUNCTIONS OF CONTROLS AND TERMINALS

2-6. Figure 2-1 shows the controls and terminals of the Model 720A and describes their functions.

2-7. RATIO ERRORS CAUSED BY LOADING OR LEAKAGE

2-8. Measurements of any kind require a knowledge of the errors associated with the equipment used to perform the measurement. Measurement made with the Model 720A are not different.

2-9. One very important source of error in measurements employing the Model 720A is the effect that external load and leakage resistances have on overall accuracy. If excessive current is drawn from the divider output tap because of loading or leakage, linearity errors which far exceed the linearity specifications can result. For this reason, Kelvin-Varley dividers customarily are used in null-balance systems in which minimum current is drawn from the divider output tap.



①	FUNCTION SWITCH	Places instrument in operating mode, or performs internal switching for calibration, or performs internal switching for decade linearity test.
②	DIALS	Decade switches are used to set the ratio of output to input (division ratio).
③	OUTPUT TERMINALS	Provide output voltage of the divider. LOW OUTPUT terminal is connected to LOW INPUT terminal through low compensating resistance.
④	BRIDGE POWER TERMINALS	Used to connect the bridge power for calibration. BRIDGE POWER (-) terminal is used for low input during decade linearity testing.
⑤	BRIDGE DETECTOR TERMINALS	Used to connect null detector for calibration.
⑥	INPUT TERMINALS	Used to connect the input voltage across the resistance of the divider.
⑦	BRIDGE BALANCE CONTROL	Used to balance bridge during self-calibration and calibration.

Figure 2-1. FUNCTIONS OF CONTROLS AND TERMINALS

2-10. Loading Errors

2-11. Figure 2-2 illustrates the Thevinin equivalent for the Model 720A Kelvin-Varley Divider.

To calculate the error in output voltage, as a fraction of the input voltage, the following expressions are given.

$$E_o (1 + \epsilon_o) = \frac{S(1 + \epsilon) E_{IN} R_L}{R_L + R_o}$$

but $E_o = SE_{IN}$

therefore $(1 + \epsilon_o) = \frac{(1 + \epsilon) R_L}{R_L + R_o}$

If $R_L \gg R_o$ and $\left(1 + \frac{R_o}{R_L}\right)$ is expanded in series then

$$(1 + \epsilon_o) = (1 + \epsilon) \left[1 - \frac{R_o}{R_L} + \left(\frac{R_o}{R_L}\right)^2 - \left(\frac{R_o}{R_L}\right)^3 + \dots \right]$$

$$\approx (1 + \epsilon) \left(1 - \frac{R_o}{R_L}\right)$$

$$\epsilon_o \approx \epsilon - \frac{R_o}{R_L}$$

and $\epsilon_L \approx \frac{R_o}{R_L}$

Converting to errors expressed as a fraction of the input voltage the expression becomes:

$$\epsilon'_o = \epsilon' - \frac{S R_o}{R_L}$$

If the 1.1 INPUT terminal is used then:

$$E_o = \frac{S}{1.1} E_{IN}$$

and:

$$\epsilon'_o \approx \epsilon' - \frac{S R_o}{1.1 R_L}$$

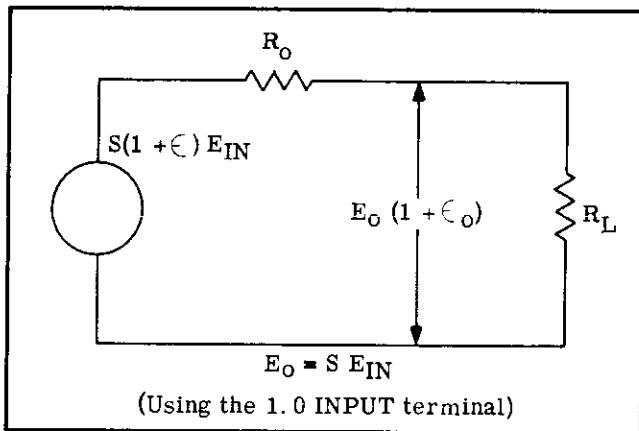


Figure 2-2. THEVININ EQUIVALENT CIRCUIT

2-12. The following list of definitions are given for the terms used in the preceding paragraphs.

- a. E_o - Nominal output voltage.
- b. E_{IN} - Input voltage.
- c. ϵ_o - Error in output voltage as a fraction of output.
- d. ϵ - Divider linearity error as a fraction of output.
- e. ϵ_L - Loading error as a fraction of output.
- f. ϵ'_o - Error in output voltage as a fraction of input.
- g. ϵ' - Divider linearity error as a fraction of input.
- h. ϵ'_L - Loading error as a fraction of input.
- i. S - Divider dial setting.
- j. R_o - Divider output resistance.
- k. R_L - Load resistance (including leakage resistance from the tap terminal to the divider input terminal).

2-13. Output Resistance Versus Loading

2-14. The graph in Figure 2-3 illustrates the approximate variation of output resistance with the dial setting for both the 1.0 and 1.1 INPUT terminals. This resistance is measured by shorting the input high and input low terminals and measuring the resistance between the output high and low terminals. When computing correction factors for loading of a particular instrument do not use the approximate resistance values given by Figure 2-3. Instead, measure the output resistance at the desired dial setting. The maximum amount of loading which will still be negligible for any dial setting may be calculated as follows:

- a. Divider specification = 0.1 ppm of input.
- b. Maximum loading error limit = 0.03 ppm of input.
- c. $\frac{S R_o}{R_L} = \epsilon_L = 0.3 \times 10^{-8}$
- d. Maximum $R_o = 66$ kilohms when $S = .454$.
- e. Minimum $R_L = \frac{S R_o}{\epsilon_L} = \frac{(.454)(6.6 \times 10^4)}{3 \times 10^{-8}}$
 $= 1 \times 10^{12}$ ohms.

2-15. Similar calculations have been made for other dial settings and the results have been plotted in Figure 2-4. The choice of a loading error limit of 0.03 ppm was, of course, arbitrary and should vary over a wide range for different measurement applications. In general, the error should be calculated and allowances made unless the errors are small compared to either the desired measurement accuracies or the divider specifications.

2-16. It should be noted that resistances calculated are the parallel combinations of the load resistor and any leakage resistances which may exist from the tap point (OUTPUT HIGH terminal) to the input terminals of the divider.

2-17. In applications where the load resistance must be supplied with a current, this current may be supplied by either a stable power supply or a second voltage divider in parallel with the measurement divider.

2-18. TEMPERATURE CONTROL

2-19. Because of slight differences in temperature coefficients of the resistors used in the Model 720A, the linearity of the divider will vary with ambient temperature. This change in linearity will never exceed ± 0.1 ppm of input per degree centigrade for dial settings above 0.1, and typically will be 0.05 ppm/ $^{\circ}$ C. For measurement applications which require the best possible accuracy, temperature and temperature variations must be considered. The operating temperature should be within 1° C of the self-calibration temperature if at all possible. If the desired operating temperature is

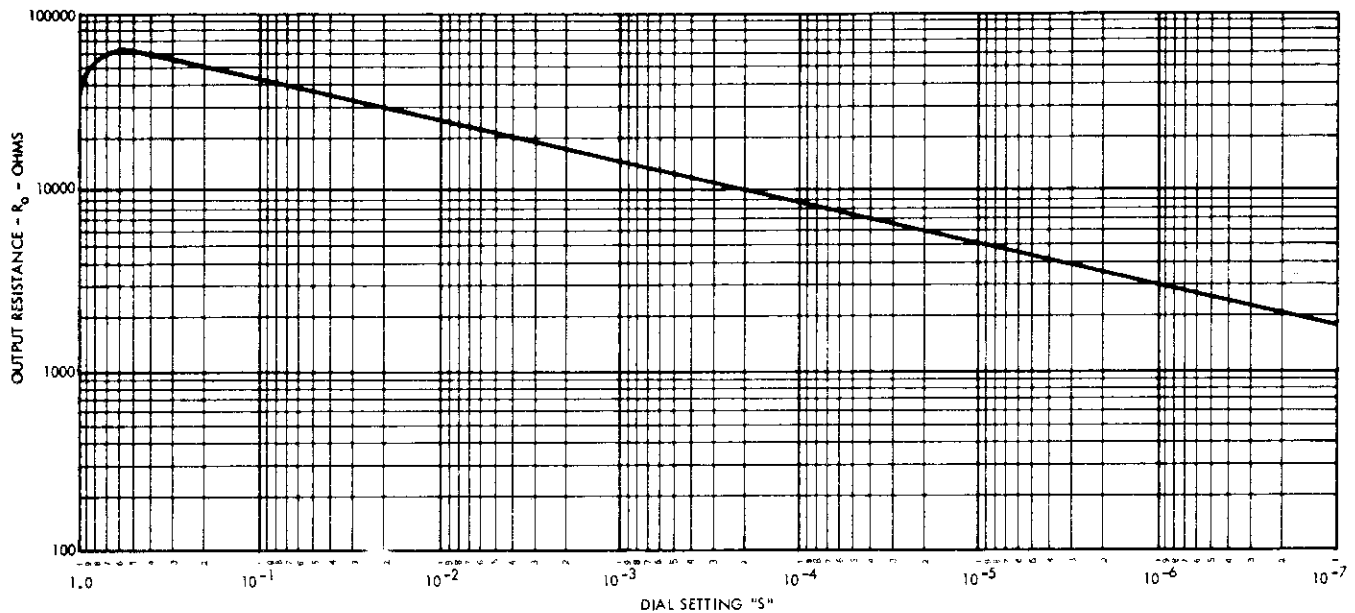


Figure 2-3. APPROXIMATE VARIATION OF OUTPUT RESISTANCE WITH DIAL SETTING

appreciably different from the last calibration temperature, the instrument should be allowed to stabilize at the operating temperature and then the self-calibration procedure should be performed to adjust linearity to 0.1 ppm of input. The Model 720A is factory tested at a temperature of $23 \pm 1^\circ\text{C}$.

2-20. POWER COEFFICIENT

2-21. The power coefficient will not exceed 0.2 ppm per watt of input power and typically will be 0.1 ppm per watt or less. With high-voltage applied, self-heating will cause the linearity of the instrument to drift. This drift may continue for as long as four hours after application of the high voltage. Low-voltage, high-accuracy measurements (0.1 ppm) should not be attempted immediately after high-voltage use. Each time the setting of the "A" decade is changed, the power distribution in it is changed because the current through the instrument is divided between the two shunted resistors of the "A" decade and the resistance of the other decades which shunts them. Because of this current division, the two shunted resistors do not become as hot as the other resistors in the "A" decade. The change in current distribution brought about by changing the setting of the "A" decade causes linearity to drift for a few minutes if high voltage is applied.

2-22. END ERRORS

2-23. When the Model 720A is compared to another divider, and a lead compensator such as the Fluke Model 721A is used, absolute linearity may be used directly without correction for end errors. In other applications, the use of a lead compensator is not practical and end error corrections must be applied. Use the following procedure to determine the end error corrections for the Model 720A:

- a. Connect the equipment as shown in Figure 2-5 (A).
- b. Adjust the input voltage to 1000 volts.
- c. With all dials set to zero, measure the voltage between the OUTPUT HIGH terminal and the INPUT LOW terminal. This is the zero error at input low. One microvolt equals 0.001 ppm.
- d. Connect the equipment shown in Figure 2-5 (B).
- e. Adjust the input voltage to 1000 volts.
- f. With all dials set to zero, measure the voltage between the OUTPUT HIGH and OUTPUT LOW terminals. This is the zero error at output low. One microvolt equals 0.001 ppm.
- g. Connect the equipment as shown in Figure 2-5 (C).
- h. Adjust the input voltage to 1000 volts.
- i. With dials set to 999999X, measure the voltage between the OUTPUT HIGH and 1.0 terminals. This is the full-scale error. One microvolt equals 0.001 ppm.
- j. Maintain the test set up of Figure 2-5 (C) except move the two leads connected to the 1.0 INPUT terminal to the 1.1 INPUT terminal.
- k. Adjust the input voltage to 1000 volts.
- l. With all dials set to 1.0 099999X, measure the voltage between the OUTPUT HIGH and 1.1 INPUT terminals. One microvolt equals 0.001 ppm.

2-24. SELF-CALIBRATION PROCEDURE

2-25. Performing this self-calibration procedure adjusts the step resistance and overall resistance of the

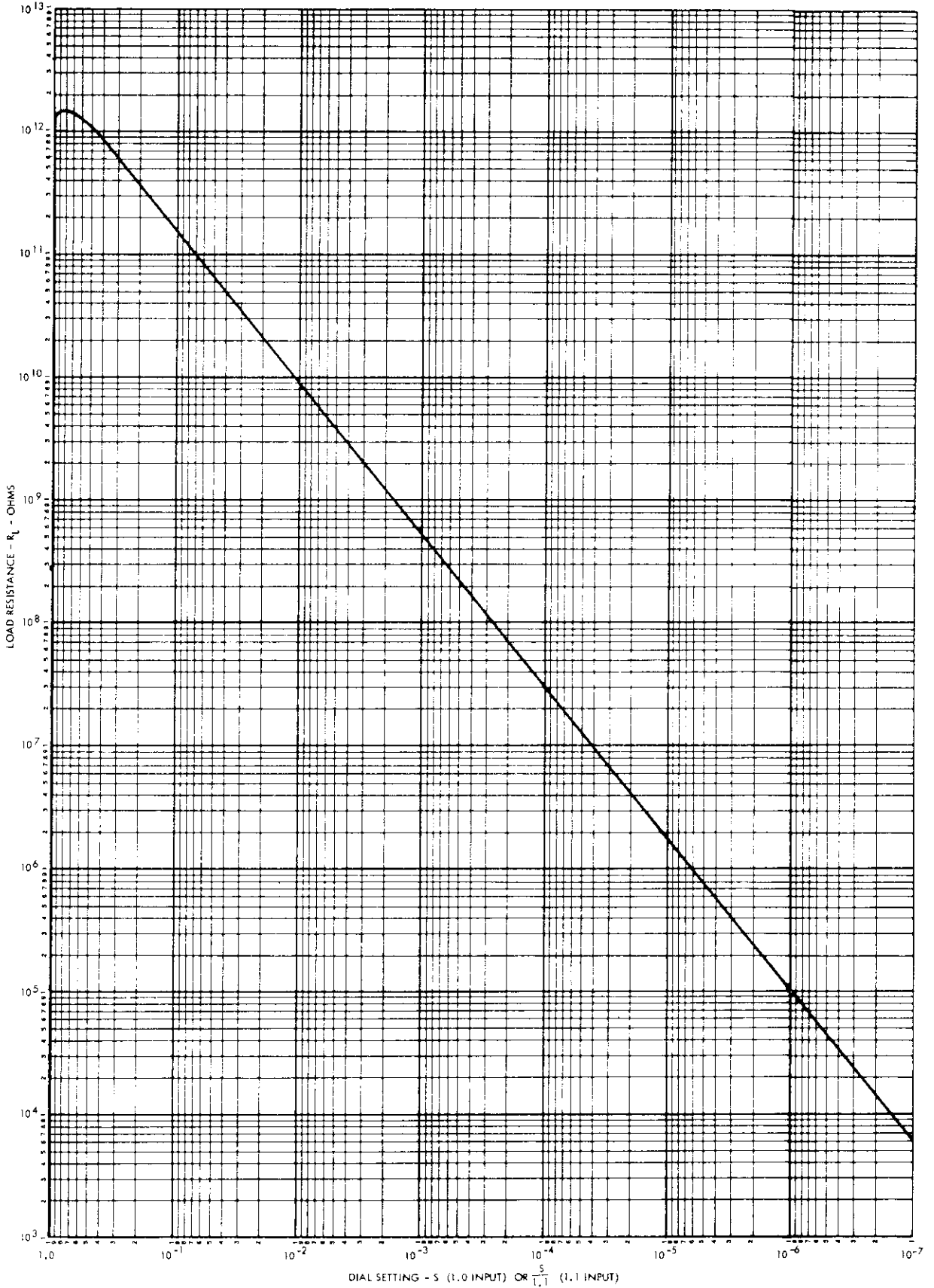


Figure 2-4. APPROXIMATE VARIATION OF MINIMUM LOAD RESISTANCE FOR 0.03 PPM OF INPUT LOADING ERROR

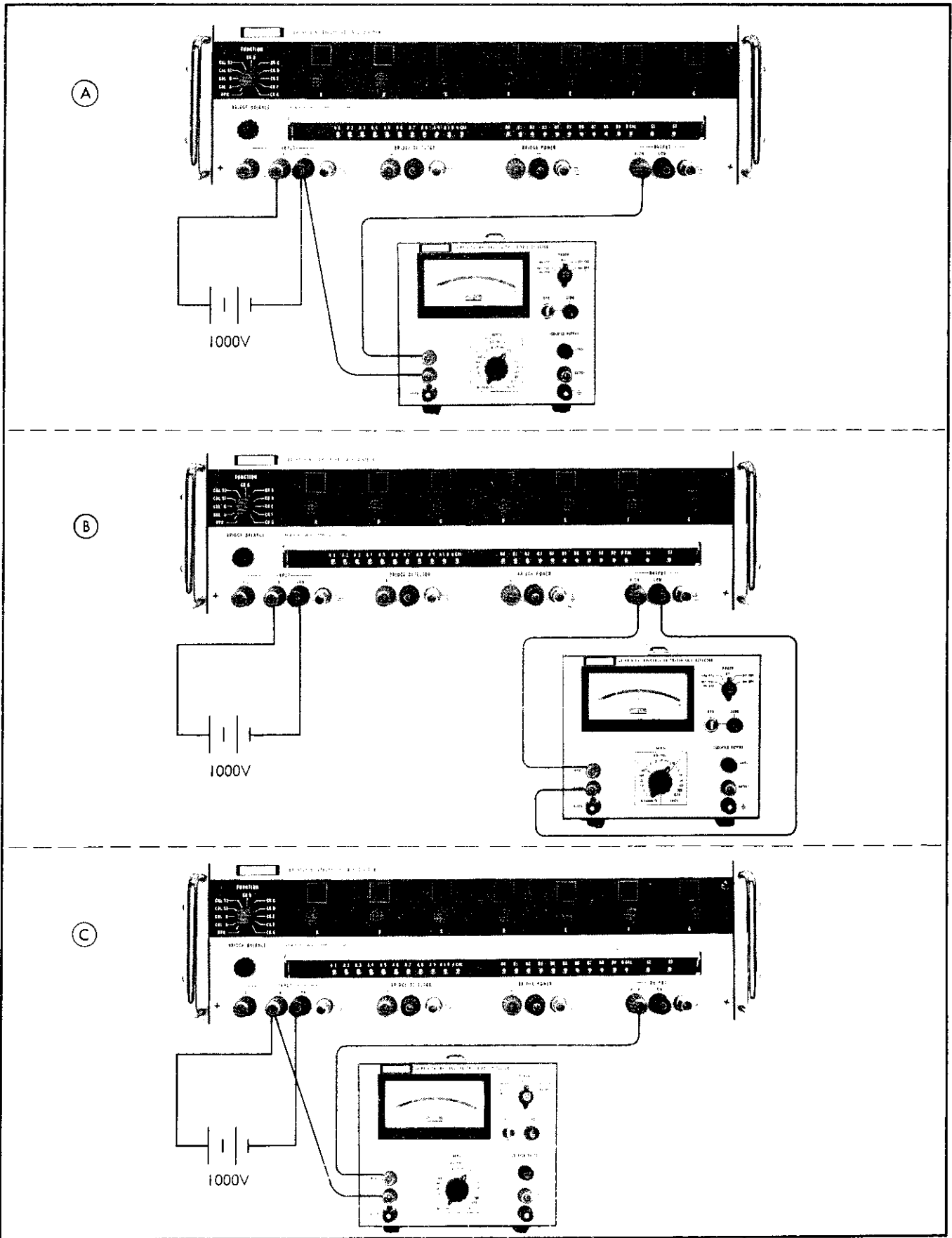


Figure 2-5. CONNECTIONS FOR DETERMINING END ERRORS

first two decades to compensate for any resistance changes caused by temperature changes or aging. Thus, the absolute linearity of the instrument is adjusted to 0.1 ppm of input. The only external test units required are a stable source of 10 volts and 20 volts such as the Fluke Model 412B and a sensitive null detector such as the Fluke Model 845AB. The procedure may be adapted easily to use batteries as the voltage source if a suitable dc power supply is not available. The procedure is as follows:

- a. Connect the null detector (845AB) to the BRIDGE DETECTOR binding posts using low thermal leads.
- b. On the Model 720A, set the FUNCTION switch to CAL A and the decade readout to .0000000.
- c. On the Model 845AB, set the range switch to 10 microvolts; set the OPR ZERO switch to ZERO and adjust for zero meter deflection. Return the OPR-ZERO switch to OPR position.
- d. Set the power supply (412B) for 20 volts output and connect it to the BRIDGE POWER binding posts.
- e. Adjust the BRIDGE BALANCE control for a null indication on the Model 845AB.
- f. Advance the "A" decade to 0.1, and adjust the associated variable resistor (A.1) to produce null, ± 0.5 microvolts.

NOTE!

As the procedure is continued, occasionally return the "A" decade switch to zero and recheck bridge balance.

- g. In turn, advance the "A" decade one position (A.2 through A CAL) and adjust the associated variable resistor.
- h. Return the "A" decade to zero upon completion of the CAL position adjustment.
- i. Set the power supply output to 10 volts.
- j. Adjust the BRIDGE BALANCE to obtain a null.

- k. Set the FUNCTION switch to CAL B, and adjust the associated variable resistor (B0) to produce a null ± 1 microvolt.

NOTE!

As the procedure is continued, occasionally return the FUNCTION switch to CAL A and recheck bridge balance.

- l. In turn, advance the "B" decade one position (B1 through B CAL) and adjust the associated variable resistor.
- m. Return the "B" decade to zero upon completion of the CAL position adjustment.
- n. Set the FUNCTION switch to CAL S1 and adjust variable resistor S1 for a null, ± 1 microvolt.
- o. Set the power supply to 20 volts.
- p. Set the "A" decade to .0 and set the FUNCTION switch to CAL A.
- q. Adjust the BRIDGE BALANCE control for a null.
- r. Set the FUNCTION switch to CAL S2 and adjust variable resistor S2 for a null, ± 0.5 microvolt.
- s. Set the FUNCTION switch to OPR and disconnect the test units. The self-calibration is complete.

2-26. CHECK POSITIONS OF THE FUNCTION SWITCH

2-27. Check positions (CK B etc.) are provided on the FUNCTION switch to permit checking the linearity of each decade from the front panel. This linearity check is a maintenance procedure. It should not be undertaken as a part of operation.

2-28. APPLICATIONS OF THE MODEL 720A

2-29. The following paragraphs give general instructions and equipment connections for calibrating a voltage divider, measuring unknown voltages, and measuring unknown resistances. Although these are by no means

TYPICAL EQUIPMENT	REQUIRED SPECIFICATIONS
DC Voltage source; John Fluke Mfg. Co. Model 332B or equivalent.	Output voltage from 0 to 1100 volts. Stability of 0.0015% per hour. Output ripple less than 40 uv rms.
DC Null Detector; John Fluke Mfg. Co. Model 845AB or equivalent.	1 uv full-scale sensitivity. 10 megohms input resistance.
Lead compensator; John Fluke Mfg. Co. Model 721A	Resolution of 0.1 milliohm.

Figure 2-6. TYPICAL ASSOCIATED EQUIPMENT FOR VOLTAGE DIVIDER CALIBRATION

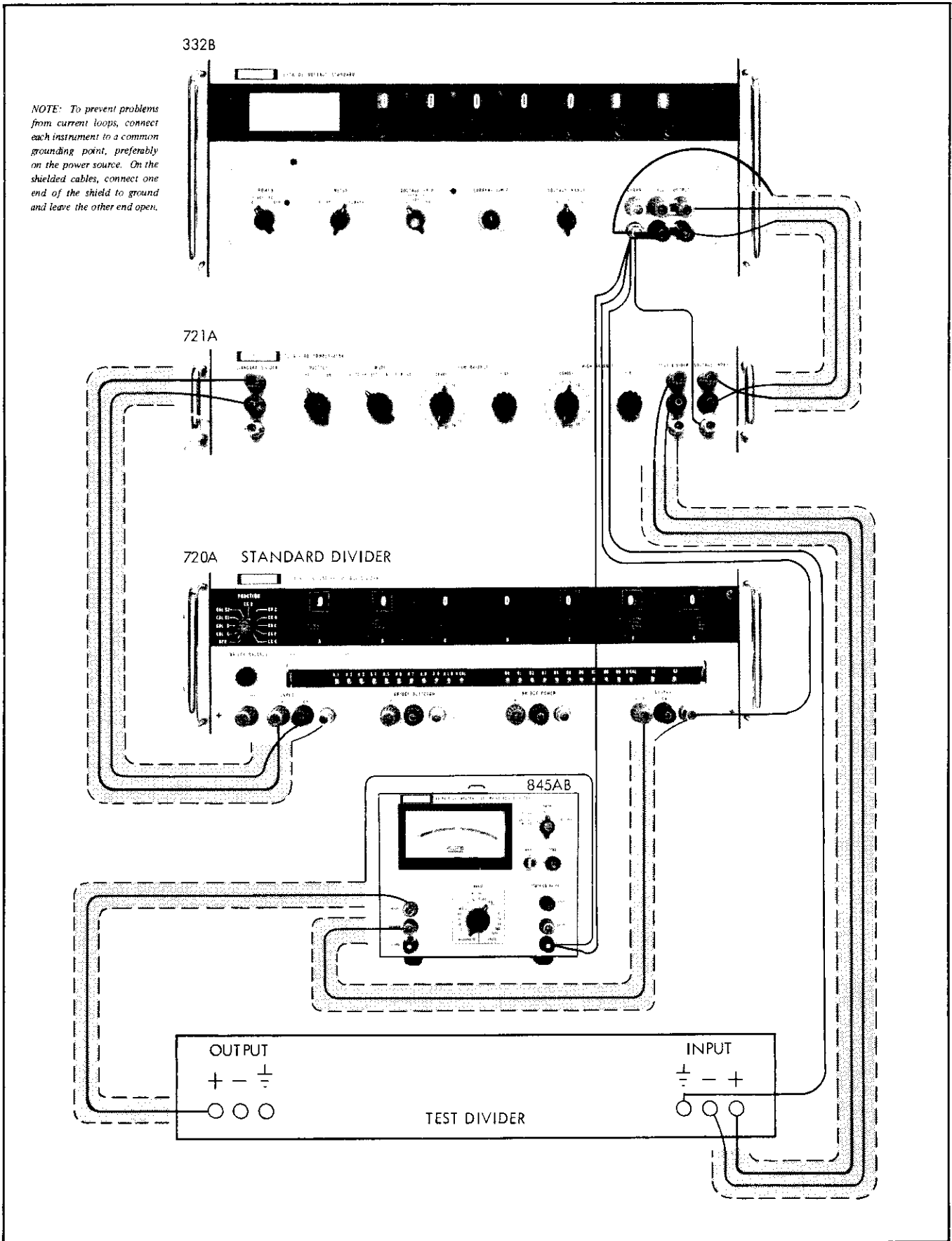


Figure 2-7. EQUIPMENT CONNECTIONS FOR CALIBRATING A VOLTAGE DIVIDER

the only applications of the instrument, they are the most common applications of a high-accuracy Kelvin-Varley divider such as the Model 720A.

2-30. Calibrating a Voltage Divider

2-31. The Model 720A in company with a dc voltage source, a null detector, and a lead compensator can be used to calibrate voltage dividers to an accuracy of 0.1 parts per million of input. Typical associated equipment for this application is listed in Figure 2-6. With this equipment, the full electrical capabilities of the Model 720A Kelvin-Varley Voltage Divider may be realized.

2-32. To calibrate a voltage divider, connect the equipment as shown in Figure 2-7 and proceed as follows:

NOTE!

Figure 2-8 is a schematic diagram of the test setup obtained by interconnecting the equipment as shown in Figure 2-7.

- a. Set both dividers to zero.
- b. Turn all equipment on and allow it to warm up until it reaches temperature equilibrium.
- c. Place the null detector in zero mode, adjust it for zero deflection, and return it to operating mode.
- d. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- e. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- f. Set both dividers to full scale and adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- g. Set both dividers to zero and re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- h. Set both dividers to the first calibration point.
- i. Observe the null detector and adjust the Model 720A to obtain a zero indication on the null detector. The difference between the setting of the Model 720A and the nominal value of the calibration point is the error of the divider being calibrated expressed as a decimal fraction of the input.
- j. Find the error at each calibration point until the calibration is complete.

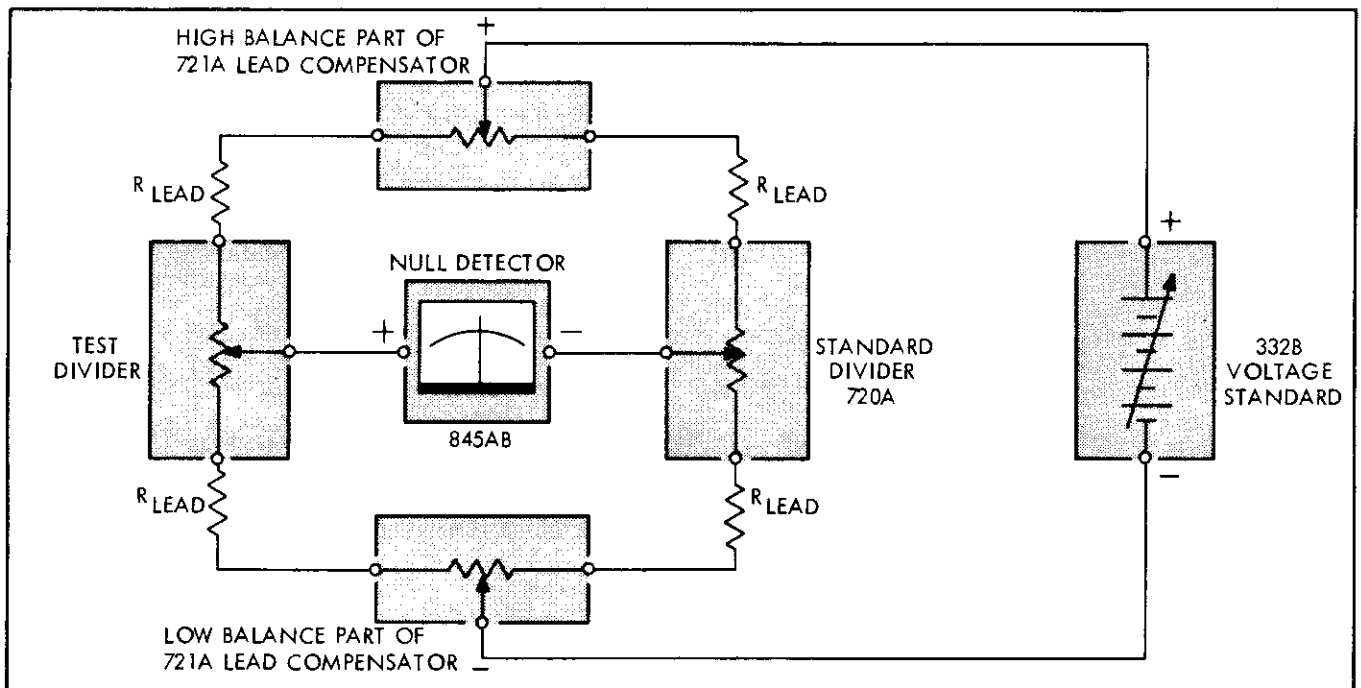


Figure 2-8. SIMPLIFIED SCHEMATIC DIAGRAM OF VOLTAGE DIVIDER CALIBRATION

NOTE!

If the dividers are set from one calibration point to the next while the test setup is energized, the null detector meter will require several seconds to recover between readings. Measurement may be performed more rapidly if the VOLTAGE switch of the lead compensator is turned to OFF before switching. Measurement may be speeded further by turning the ZERO-OPR switch of the null detector to ZERO during switching. This prevents the transient caused by turning the voltage on, from saturating the null detector amplifier.

TYPICAL EQUIPMENT	REQUIRED SPECIFICATIONS
DC Voltage Source; John Fluke Mfg. Co. Model 332B or equivalent.	Output voltage from 0 to 1100 volts. Stability of 0.0015% per hour. Output ripple less than 40 uv rms.
DC Null Detector (2 required); John Fluke Mfg. Co. Model 845AB or equivalent.	1 uv full-scale sensitivity. 10 megohms input resistance.
Standard Cell; Guildline Instruments Model 9152 or equivalent.	At least three saturated cells. Accuracy of 0.0005%.
DC Reference Voltage Divider; John Fluke Mfg. Co. Model 750A or equivalent.	Output accuracy of ± 10 ppm. Input and output voltage. Rating of 1100V dc.

Figure 2-9. TYPICAL ASSOCIATED EQUIPMENT FOR MEASURING UNKNOWN VOLTAGES

2-33. Measuring Unknown Voltages

2-34. The Model 720A in company with a stable dc voltage source, two null detectors, a standard cell, and a reference voltage divider may be used to measure an unknown voltage with high accuracy. Typical equipment for this application is listed in Figure 2-9. With this equipment the full electrical capabilities of the Model 720A may be realized.

2-35. To measure an unknown voltage, first connect the equipment as shown in Figure 2-10. The size of wire for leads A and B should be no smaller than No. 24 and the total length should be less than 3 feet. Then measure the approximate voltage by dialing the Model 720A to .0000000 and reading the null detector on the appropriate voltage range. Proceed as follows:

- a. Open the standard cell voltage switch on the reference divider and set the standard cell voltage dials to the correct standard cell voltage.
- b. Set the reference divider input switch to the first position higher than the voltage to be measured. Set the output switch to the same position.
- c. Turn on all equipment and allow it to warm up until it reaches temperature equilibrium.
- d. Set the standard cell switch of the reference divider to momentary position and adjust the output of the dc source to obtain a null indication on null detector number 1.
- e. Adjust the readout dials of the Model 720A to obtain a null indication on null detector number 2.
- f. Calculate the unknown voltage by multiplying the input voltage of the Model 720A by the numerical setting of the readout dials. For example, if the input voltage is 100 volts and the dial setting is .8903174, the unknown voltage is 89.03174 volts.

2-36. Simplified Method of Voltage Measurement

2-37. Voltages under 11 volts may be measured with comparable accuracy by the simpler equipment setup shown in Figure 2-12. This method standardizes the output voltage of the Model 720A by comparing it directly to a known standard cell. When used with an input of 1.1 volts, it is ideally suited to the accurate certification of standard cells. Typical associated equipment for this application is listed in Figure 2-11.

2-38. To measure the unknown voltages, connect the equipment as shown in Figure 2-12 and proceed as follows:

- a. Set the dc voltage source for an output of eleven or 1.1 volts depending on the desired range and allow to warm up.
- b. Set the readout dials of the Model 720A to the standard cell voltage.
- c. Connect the standard cell in place of the unknown voltage and adjust the dc source to obtain a null indication on the null detector.
- d. Disconnect the standard cell.
- e. Set the readout dials of the Model 720A to the approximate value of the unknown voltage.
- f. Connect the unknown voltage.
- g. Adjust the readout dials of the Model 720A to obtain a null indication on the null detector.
- h. Calculate the unknown voltage by multiplying by 10 or 1 depending on the range. For example, if the readout dials are set at .7500055 and the input is 11 volts, the unknown voltage is 7.500055 volts.

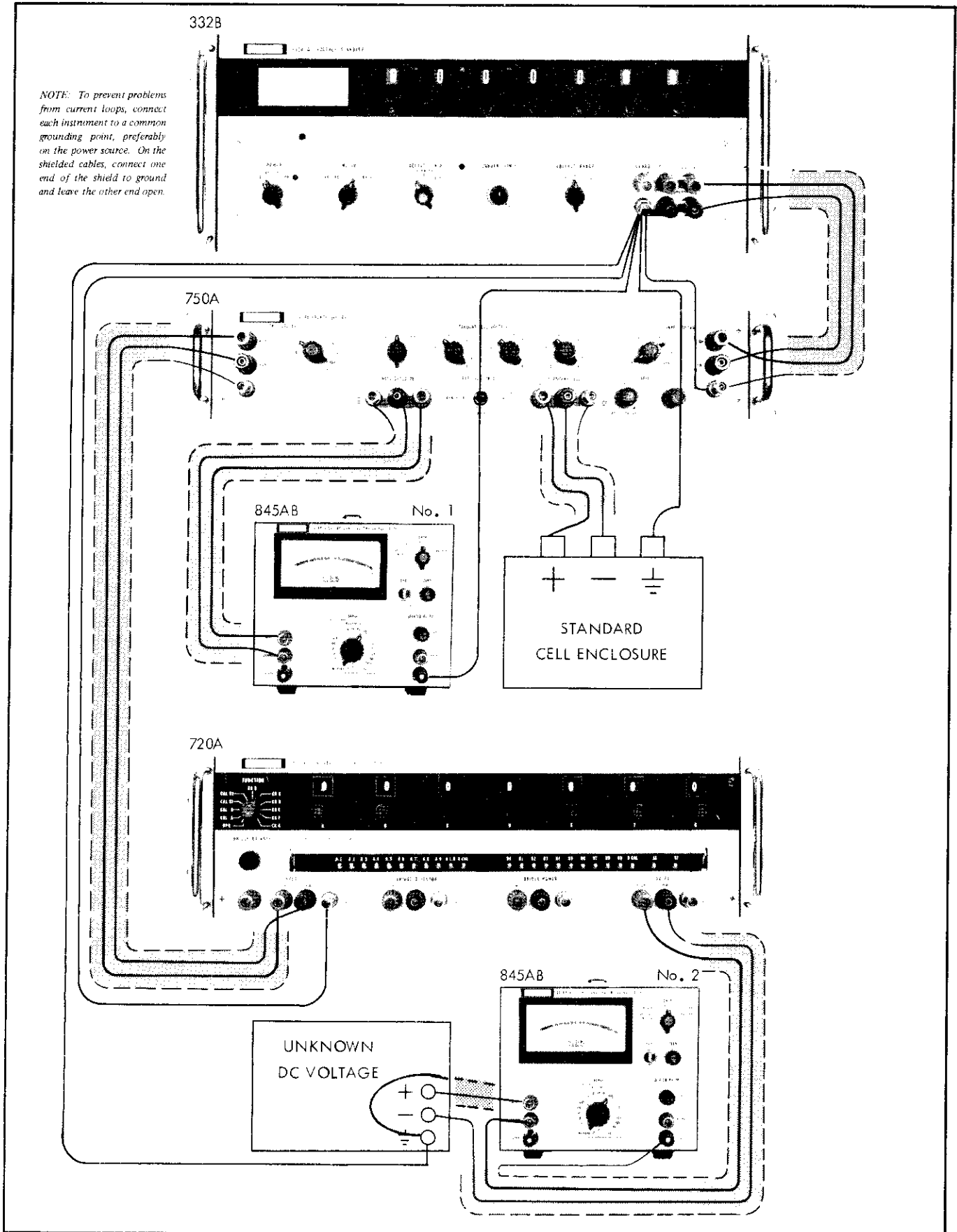


Figure 2-10. EQUIPMENT CONNECTIONS FOR VOLTAGE MEASUREMENTS (Sheet 1 of 2)

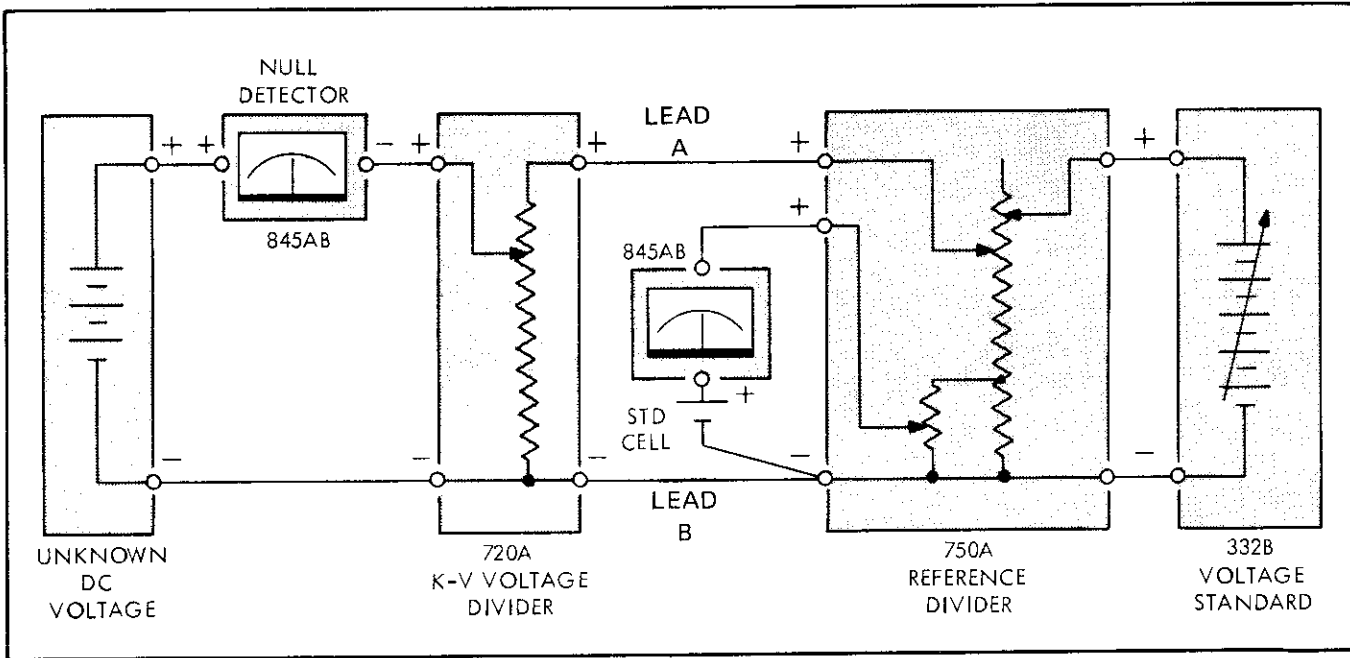


Figure 2-10. EQUIPMENT CONNECTIONS FOR VOLTAGE MEASUREMENTS (Sheet 2 of 2)

2-39. Measuring Unknown Resistance

2-40. The Model 720A may be used in a setup including a null detector, a power supply, and a standard resistor, to measure an unknown resistance with a high degree of accuracy. Typical associated equipment for this application is listed in Figure 2-13. The unknown resistance and the standard resistance should be in the same order of magnitude for the best accuracy.

2-41. To measure an unknown resistance, connect the equipment as shown in Figure 2-14 using shielded leads. Apply the positive lead from the dc voltage source to the 1.0 INPUT terminal of the Model 720A. Proceed as follows:

P_1 , P_2 , P_3 , and P_4 = decimal ratio set on the readout dials of the Model 720A at points P_1 , P_2 , P_3 , and P_4 respectively.

If $R_x + R_{std}$ is greater than 100 ohms, the use of a lead compensator is desirable. If a lead compensator is used, P_1 can be made equal to 1.0000000 and P_4 can be made equal to .0000000.

$$\frac{R_x}{R_{std}} = \frac{1 - P_2}{P_3}$$

If lead resistance between the resistors is made insignificant in addition to using a lead compensator, then $P_2 = P_3$ and the equation may be further simplified to:

$$\frac{R_x}{R_{std}} = \frac{1}{P} - 1$$

- a. Set the dc voltage source to the desired test voltage.

CAUTION!

Do not exceed the current rating of the standard resistor.

- b. Set the readout dials of the Model 720A to zero.
- c. Connect the null detector lead to point P_1 and adjust the readout dials of the Model 720A to obtain a null indication. Record the dial reading.

TYPICAL EQUIPMENT	REQUIRED SPECIFICATIONS
DC Voltage Source; John Fluke Mfg. Co. Model 332B or equivalent.	Output voltage from 0 to 1100 volts. Stability of 0.0015% per hour. Output ripple less than 40 uv rms.
DC Null Detector John Fluke Mfg. Co. Model 845AB or equivalent.	1 uv full-scale sensitivity. 10 megohms input resistance.

Figure 2-11. TYPICAL ASSOCIATED EQUIPMENT FOR MEASURING UNKNOWN VOLTAGES

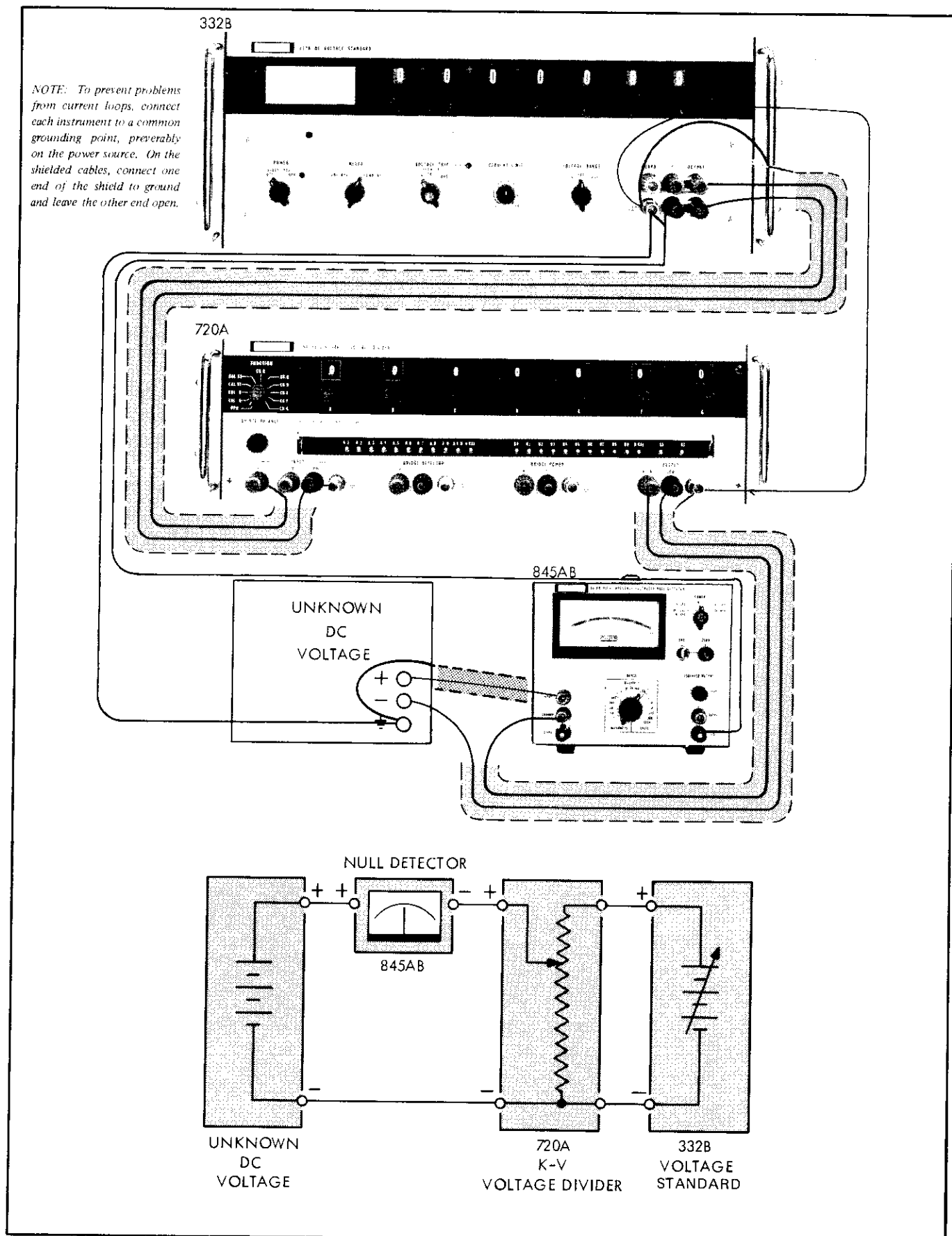


Figure 2-12. EQUIPMENT CONNECTIONS FOR SIMPLIFIED METHOD OF VOLTAGE MEASUREMENT

TYPICAL EQUIPMENT	REQUIRED SPECIFICATIONS
DC Voltage Source; John Fluke Mfg. Co. Model 332B or equivalent.	Output voltage from 0 to 1100 volts. Stability of 0.0015% per hour. Output ripple less than 40 uv rms.
DC Null Detector John Fluke Mfg. Co. Model 845AB or equivalent.	1 uv full-scale sensitivity. 10 megohms input resistance.
Standard resistor.	

Figure 2-13. TYPICAL ASSOCIATED EQUIPMENT FOR MEASURING UNKNOWN RESISTANCE RATIOS

- d. Move the null detector lead to point P_2 , adjust the readout dials to obtain a null, and record the dial reading.
- e. Move the null detector lead to point P_3 , adjust the readout dials to obtain a null, and record the reading.
- f. Move the null detector lead to point P_4 , adjust the dials to obtain a null, and record the dial reading.
- g. Calculate the unknown resistance from the following equation.

$$\frac{R_x}{R_{\text{std}}} = \frac{P_1 - P_2}{P_3 - P_4}$$

where:

R_x = unknown resistance
 R_{std} = standard resistance

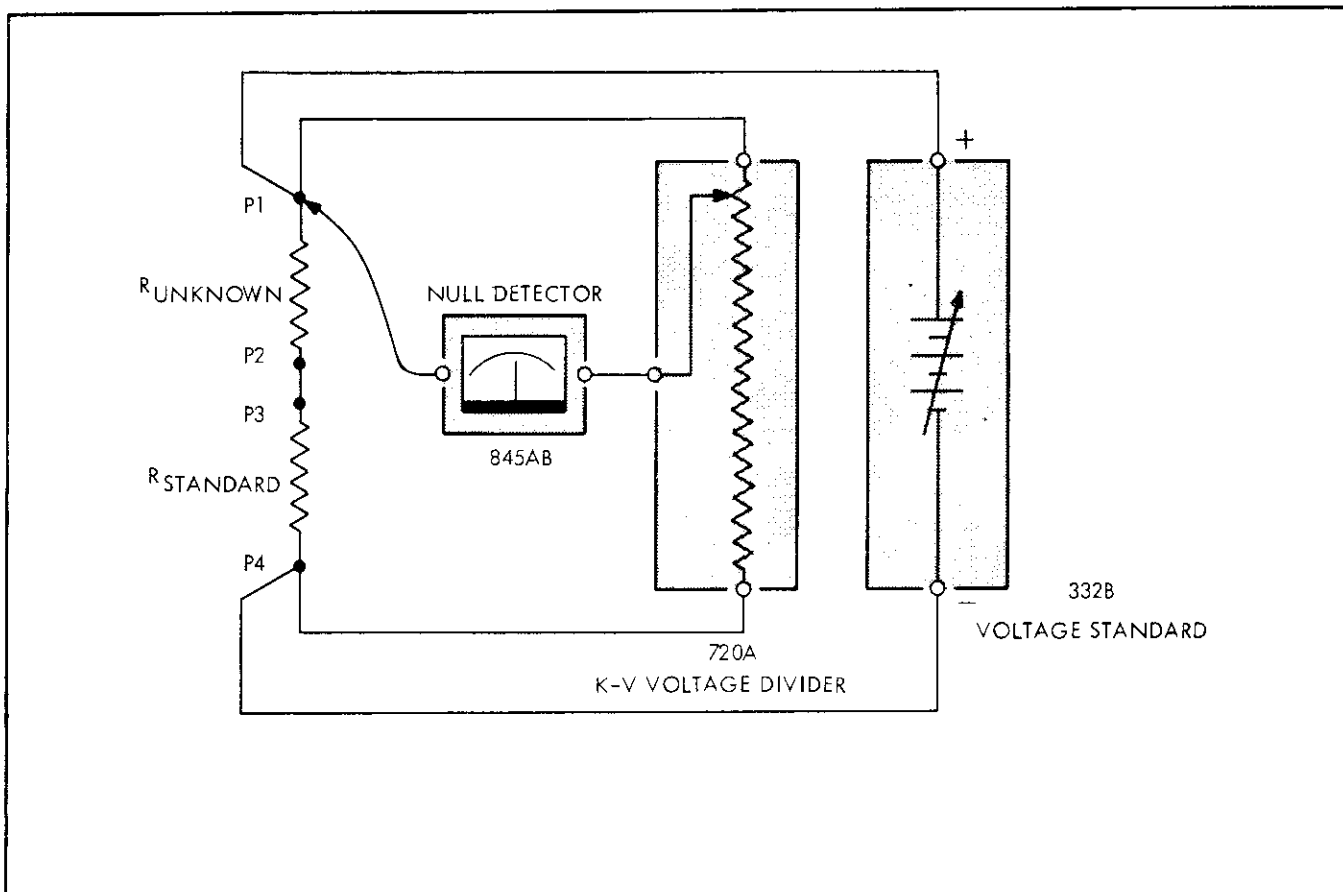


Figure 2-14. EQUIPMENT CONNECTIONS FOR DETERMINING AN UNKNOWN RESISTANCE VALUE (Sheet 1 of 2)

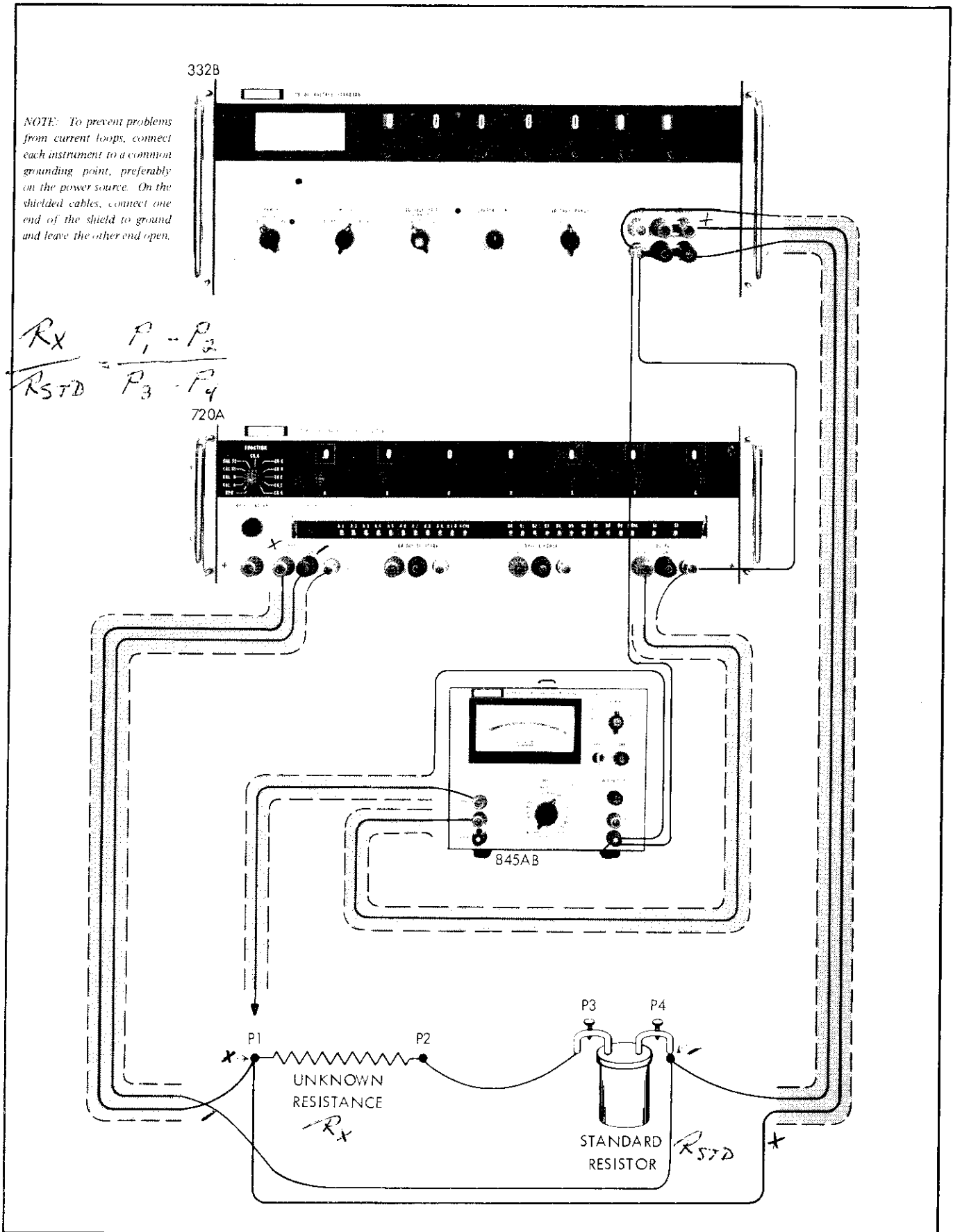


Figure 2-14. EQUIPMENT CONNECTIONS FOR DETERMINING AN UNKNOWN RESISTANCE VALUE (Sheet 2 of 2)

Section 3

Theory of Operation

3-1. INTRODUCTION

3-2. The Kelvin-Varley divider is a resistive circuit used primarily as a ratio standard. It is capable of dividing the input voltage with high resolution, usually to six or seven decimal places, and with high accuracy, usually a few parts per million.

3-3. THE BASIC CIRCUIT

3-4. Figure 3-1 is a simplified schematic diagram of a basic Kelvin-Varley divider. This simplified divider is capable of dividing the input voltage into 10,000 parts. It consists of four decades or resistive dividers each of which divides its input voltage into 10 equal parts ($10^4 = 10,000$).

3-5. For a decade to divide the voltage across it into 10 equal parts it must consist of 10 equal resistances. Placing the resistance of succeeding decade in parallel with a portion of the resistance of a decade, reduces the effective resistance of that portion. Referring to Figure 3-1, notice that the shunted resistance in the first decade is 20 kilohms and that each of the other steps is 10 kilohms. The 20 kilohms in the first decade is shunted by the 20 kilohms total effective resistance of the second decade resulting in a total effective resistance of 10 kilohms for that step. Thus all steps are kept equal. Each step of the second decade is two kilohms. The four kilohms spanned by the switch contacts is shunted by the four kilohms effective resistance of the third decade. Similarly 800 ohms of the third decade is shunted by the 800 ohms total resistance of the fourth decade.

3-6. CIRCUIT REFINEMENTS

3-7. Although the simplified Kelvin-Varley divider shown in Figure 3-1 shows all of the essential details of the basic circuit, a number of common design refinements should be mentioned. The latter decades may employ step resistors which are all of the same value and a shunt across the entire decade to reduce the effective decade resistance to the proper value. In Figure 3-1, this could be accomplished by using 400 ohm resistors in the fourth decade with a 1000 ohm shunt across the decade to reduce the effective resistance of

the decade to 800 ohms. This avoids the necessity of using resistors of very small value in the latter decades. Usually each step of at least the first decade will consist of two equal resistors matched for equal but opposite temperature coefficients. This matching tends to produce a zero temperature coefficient for each step and for the entire decade, which reduces the nonlinearity caused by uneven temperature when power is applied. Some Kelvin-Varley dividers have adjustable trimmer resistors in the first, or even the second and third decades to permit compensation for drift and changes of ambient temperature. Overranging capability is provided in some circuits by adding an additional step of resistance and a 1.1 input terminal at the upper end of the first decade. In some dividers a small series resistance is added between the lower end of the divider string and the low input terminal to compensate for contact and wiring resistance bringing the low output voltage at zero setting to the same value as the low input voltage. Although these refinements improve the capability of the circuit, it operates in the same manner with them as without them.

3-8. THE MODEL 720A

3-9. The Model 720A is a seven-dial Kelvin-Varley divider with overranging and adjustable trimmers in the first three decades. The low output is compensated by a small resistance in series with the low input terminal. The input resistance (total effective resistance of the first decade is 110 kilohms at the 1.1 input terminal or 100 kilohms at the 1.0 input terminal. Resistors of equal value and fixed decade shunts are used in the last four decades to avoid using very small resistance values.

3-10. Design characteristics of the Model 720A which are not commonly found in Kelvin-Varley dividers include adjustable shunts in the first three decades, a built-in Wheatstone bridge, and switching to permit linearity adjustment (self-calibration) from the front panel. In addition, internal switching provides access to the second through the seventh decades so the linearity of any decade may be checked against a 10-step divider from the front panel.

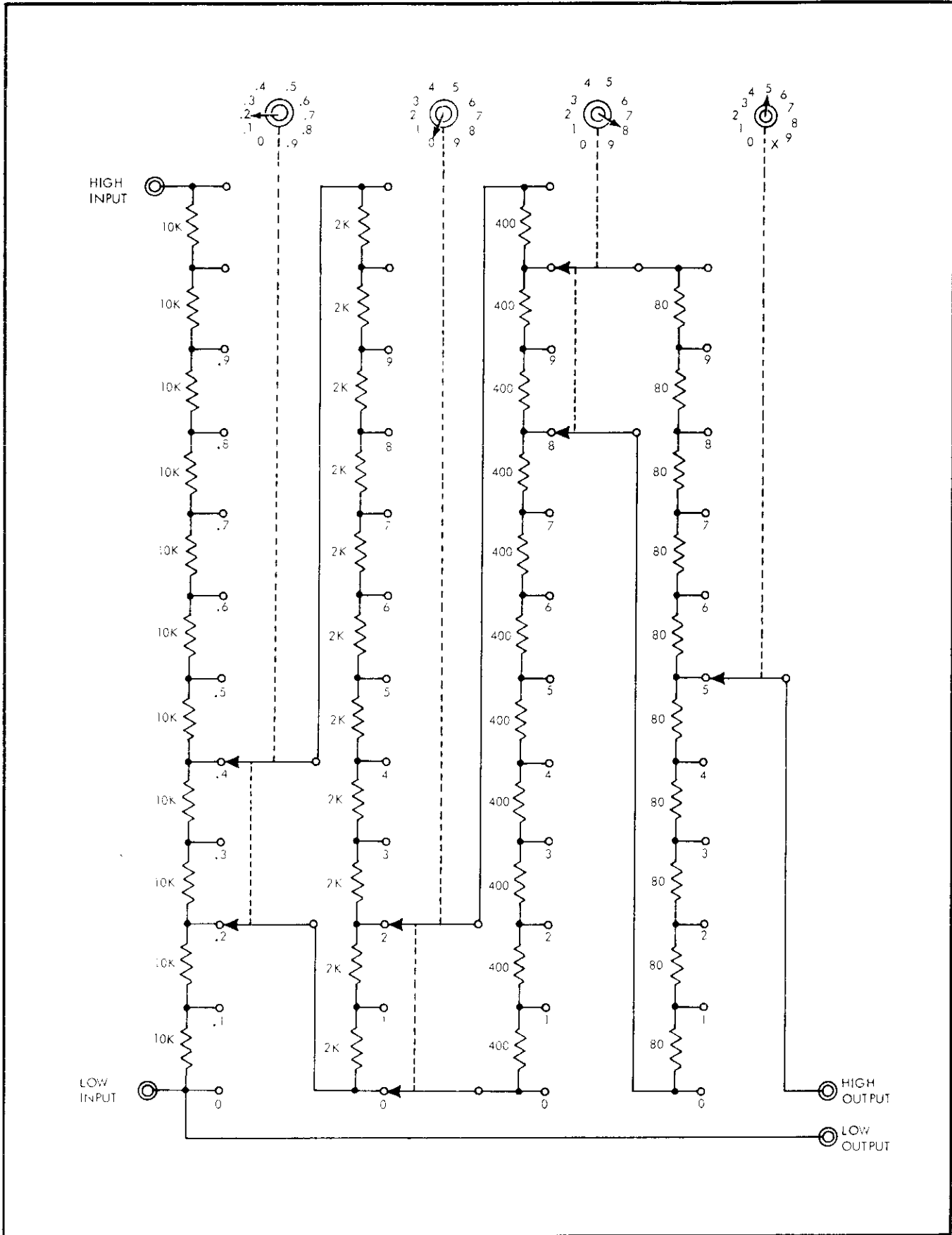


Figure 3-1. SIMPLIFIED SCHEMATIC DIAGRAM OF BASIC KELVIN-VARLEY DIVIDER CIRCUIT

Section 4

Maintenance

4-1. INTRODUCTION

4-2. This section contains the instructions and information required for maintenance of the Model 720A Kelvin–Varley Divider. Instructions are included for preventive maintenance, testing and repair of the instrument. If repair is beyond the capability of the user, it is recommended that the instrument be returned to the manufacturer. All maintenance procedures except the replacement of factory selected resistors and resistors housed in the oil tank are within the capability of a skilled technician if the listed test equipment is available.

4-3. The ratio accuracy of 0.1 ppm of the Model 720A is guaranteed for one year after shipment from the factory provided the instrument is regularly self-calibrated in accordance with paragraph 2-24 and is operated in the same environment in which it is self-calibrated. The instrument also must meet the requirements of the Leakage Resistance Test, paragraph 4-8. In the self-calibration procedure, all resistors on the A and B decades are adjusted to be equal to each other by substituting each in turn into the self-contained resistance bridge. The Linearity Test given in paragraph 4-14 should be performed once each year to verify instrument performance. If testing and calibration are beyond the capability of the user, these services may be obtained from a commercial calibration laboratory or from the manufacturer.

4-4. TEST EQUIPMENT REQUIRED FOR MAINTENANCE

4-5. The test equipment required for maintenance is listed in Figure 4-1. Equivalent or similar units may be substituted for those listed providing they have the required specifications listed in the figure.

4-6. PREVENTIVE MAINTENANCE

4-7. Preventive maintenance of the Model 720A consists of leakage resistance testing, cleaning, switch contact lubrication, and linearity testing. The frequency with which preventive maintenance procedures should be scheduled depends upon the user's requirements and the environment of the instrument. In an air conditioned standards laboratory, there will be little contamination of surfaces within this instrument and therefore testing and cleaning will seldom be required. In a contaminated atmosphere, frequent testing and cleaning may be required to maintain the accuracy of the instrument.

4-8. Leakage Resistance Tests

4-9. The need for cleaning can be determined without removing the cover from the Model 720A by performing

RECOMMENDED EQUIPMENT	SPECIFICATIONS REQUIRED
DC Voltage Source John Fluke Mfg. Co. Model 332B or Model 412B	Source of 0 to 1100 vdc. Accuracy at least 0.25% Stability at least 0.005% per hour.
DC Null Detector John Fluke Mfg. Co. Model 845AB	Sensitivity at least 10 microvolts full scale. 10 Megohm input Resistance.
Lead Compensator John Fluke Mfg. Co. Model 721A	Resolution of 0.1 milliohm. Ratio capability of 110:1
Standard Divider John Fluke Mfg. Co. Model 720A	Ratio accuracy of 0.1 ppm of input.
Standard Divider (11 Steps)	Ratio accuracy of 0.05 ppm of input
Decade Resistance Standard Electro Scientific Industries Model RS925A	4007.6 ohms, 10,000 ohms Accuracy of ± 20 ppm

Figure 4-1. TEST EQUIPMENT REQUIRED FOR MAINTENANCE

the simple leakage resistance test described in this paragraph. This test should also be performed after cleaning to assure that all contamination has been removed. To measure leakage resistance, proceed as follows:

- a. Place the Model 720A on a sheet of dielectric.
- b. Use teflon insulated wire to connect the Model 720A, a 1000-volt source (Model 332B), and a null detector (Model 845AB) as shown in Figure 4-2.
- c. Connect a shunt resistor across the input of the null-detector to bring its input resistance to one megohm on the one millivolt range. The value required for the Model 845AB is 1.1 megohms.
- d. Turn on the 1000-volt supply and read the null detector. An indication of 1 millivolt corresponds to leakage resistance of 10^{12} ohms. If the indication is more than 1 millivolt, the leakage resistance is too low and corrective measures must be taken. If repeated cleaning fails to correct the problem, troubleshooting must be undertaken.

4-10. CLEANING

- 4-11. When the Model 720A is properly cared for and

kept in a controlled atmosphere, cleaning will seldom be required. However, any contamination, particularly oil, in the instrument can contribute to reduced leakage resistance which will impair accuracy. Special care has been taken in the design and manufacture of the instrument to prevent leakage. The voltage dial switches are supported by Lexan spacers, and the circuit board is coated with a moisture sealant and isolated from the chassis by polyethylene grommets. These insulators and the switches can be contaminated easily by handling or by airborne contaminants. Dust may be removed with dry oil-free air at a pressure of 15 pounds per square inch or less. To remove oil, place the instrument on its side, place paper towels under it and spray with denatured anhydrous ethyl alcohol, Crown SPRA-TOOL No. 8011 or equivalent. When dry, perform switch contact lubrication, paragraph 4-12. After cleaning and drying, the leakage resistance test should be performed to assure that the excessive leakage has been corrected.

4-12. Switch Contact Lubrication

- 4-13. Corrosion of switch contacts can cause high contact resistance in one or more positions resulting in an impairment of linearity. If evidence of this condition is present and exercising the switch fails to correct it, the switch contact should be lubricated with a special purpose switch lubricant. The product recommended for this purpose is Rykon lubricant No. 2 EP (American Oil Co.) mixed with Tuluol. It should be carefully applied in a very thin film with a camel's hair brush.

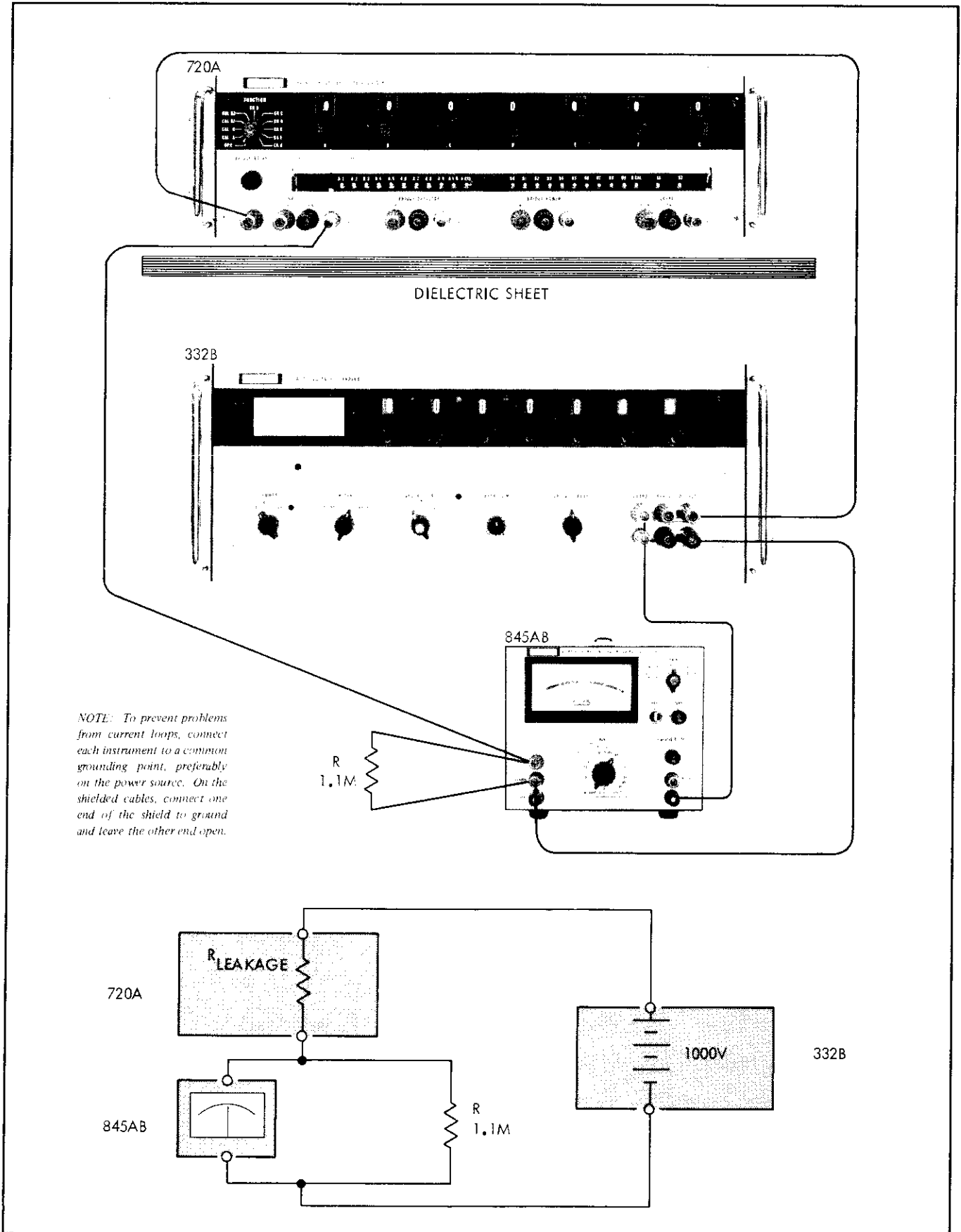


Figure 4-2. EQUIPMENT CONNECTIONS FOR LEAKAGE RESISTANCE TEST

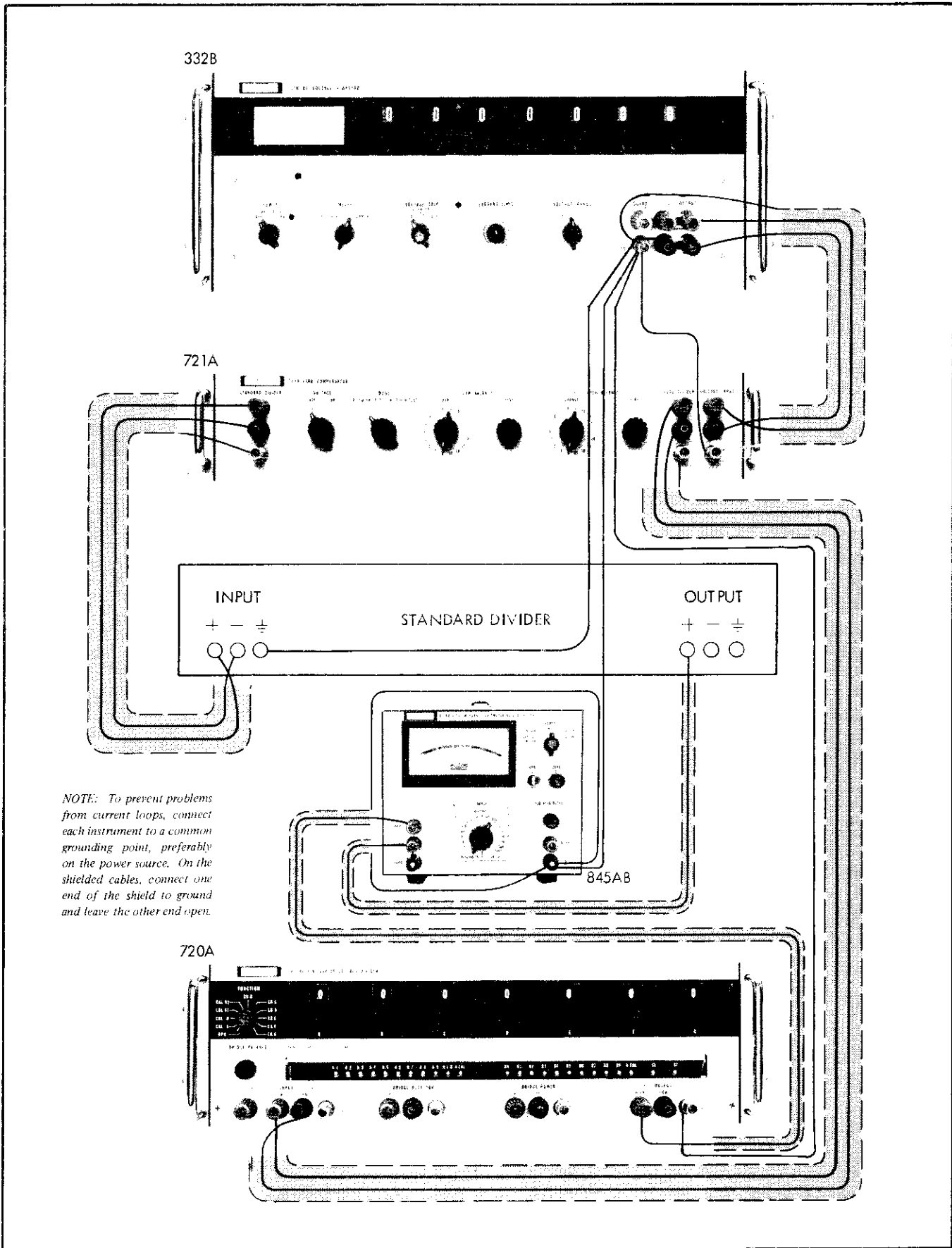


Figure 4-3. EQUIPMENT CONNECTIONS FOR LINEARITY COMPARISON TEST

CAUTION!

Great care should be used to avoid excessive use of contact lubricant on the switches of the Model 720A. The contacts should not be lubricated unless there is evidence of irregular operation.

Before applying the lubricant, clean the switch following the instructions in paragraph 4-10. Only a minute amount of lubricating fluid should be applied. After application, exercise the switch by rotating it through all positions several times.

4-14. Linearity Testing

4-15. The design of the 720A Voltage Divider is such that if the instrument is self-calibrated, if the leakage resistance is low, and if the switch contacts display repeatable contact resistance, the divider will meet its linearity specifications. Because of the extremely tight over-all specification (0.1 PPM of input) very few laboratories will have both the necessary equipment and the required technical skills to prove this. The following linearity test using a second Model 720A as a standard is therefore intended only to indicate gross errors (0.2 PPM of input) in the first decade and to prove specification on the lower decades. The customer who hopes to prove more than this is referred to the following articles and papers:

1. Andrew F. Dunn, "Calibration of a Kelvin-Varley Voltage Divider," National Research Council Report No. 7863.
2. M. L. Morgan and J. C. Riley, "Calibration of a Kelvin-Varley Standard Divider," IRE

Trans. on Instrumentation, vol. 1-9, pp 237-243; Sept. 1960.

4-16. To compare divider linearity, connect the equipment as shown in Figure 4-3 and proceed as follows:

NOTE!

Figure 4-4 is a schematic diagram of the test setup obtained by interconnecting the equipment as shown in Figure 4-3.

- a. Self-calibrate the Model 720A. (See paragraph 2-24 in Section II).
- b. Set both dividers to zero.
- c. Set the voltage source to the desired test voltage, turn on all equipment and allow it to warm up until it reaches temperature equilibrium.
- d. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- e. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- f. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.

NOTE!

If the dividers are set from one calibration point to the next while the test setup is energized, the null detector meter will require several seconds to recover between readings. Measurement may

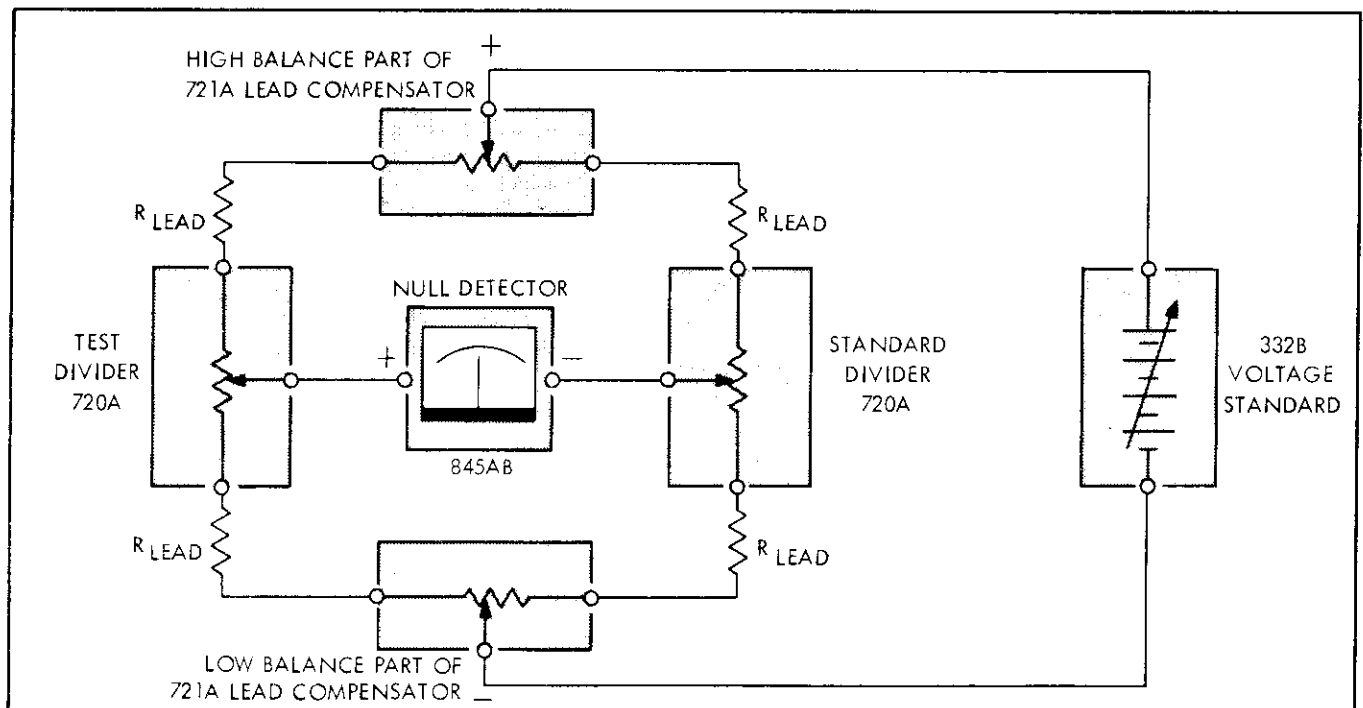


Figure 4-4. SIMPLIFIED SCHEMATIC DIAGRAM OF LINEARITY COMPARISON TEST

be performed more rapidly if the VOLTAGE switch of the lead compensator is turned to OFF before switching. Measurement may be speeded further by turning the ZERO-OPR switch of the null detector to ZERO during switching. This prevents the transient caused by turning the voltage on from saturating the null detector amplifier.

- g. Set both dividers to full scale and adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- h. Set both dividers to zero and re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- i. Set the null detector to the desired sensitivity.
- j. Set both dividers to the first comparison point and adjust the standard divider for a near zero indication on the null detector. The dial settings of the two dividers plus the null detector reading shall agree within a tolerance of 0.2 PPM. This criterion is applicable for input voltages of 100 volts or less.
- k. Continue to compare each setting of each decade until the comparison is complete. The following dial setting combinations should be checked on each decade.

0 all zeros	_____
1 all zeros	1 (dial 09 and all 9 ^s except X in last)
2 all zeros	2 (dial 19 and all 9 ^s except X in last)
3 all zeros	3 (dial 29 and all 9 ^s except X in last)
4 all zeros	4 (dial 39 and all 9 ^s except X in last)
5 all zeros	5 (dial 49 and all 9 ^s except X in last)
6 all zeros	6 (dial 59 and all 9 ^s except X in last)
7 all zeros	7 (dial 69 and all 9 ^s except X in last)
8 all zeros	8 (dial 79 and all 9 ^s except X in last)
9 all zeros	9 (dial 89 and all 9 ^s except X in last)
1.0 all zeros	10 (dial 99 and all 9 ^s except X in last)
_____	1.1 (dial 1.09 and all 9 ^s except X in last)

4-17. Decade Linearity Testing

4-18. The CK B through CK G positions of the FUNCTION switch are provided to permit access to the individual decades of the Model 720A under test so that each may be checked against the first decade of the standard divider. To test the linearity of each decade individually, proceed as follows:

- a. Change the test setup to that shown in Figure 4-5.

NOTE!

Figure 4-6 is a schematic diagram of the test setup obtained by interconnecting the equipment as shown in Figure 4-5.

- b. Turn the FUNCTION switch to CK B.
- c. Set the standard divider to zero.
- d. Set the divider under test to 1.0 000000.
- e. Set the voltage source to the desired test voltage.

CAUTION!

Do not exceed the maximum test voltages listed in Figures 4-7 through 4-12.

- f. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- g. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- h. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.

NOTE!

If the dividers are set from one calibration point to the next while the test setup is energized, the null detector meter will require several seconds to recover between readings. Measurement may be performed more rapidly if the VOLTAGE switch of the lead compensator is turned to OFF before switching. Measurement may be speeded further by turning the ZERO-OPR switch of the null detector to ZERO during switching. This prevents the transient caused by turning the voltage on, from saturating the null detector amplifier.

- i. Set the standard divider to full scale.
- j. Set the divider under test to 1.0 99999X.
- k. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- l. Set the divider under test back to 1.0 000000 and set the standard divider back to zero.
- m. Re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- n. Set the null detector for the desired sensitivity and make the linearity measurements given in Figure 4-7. The null detector indications must be

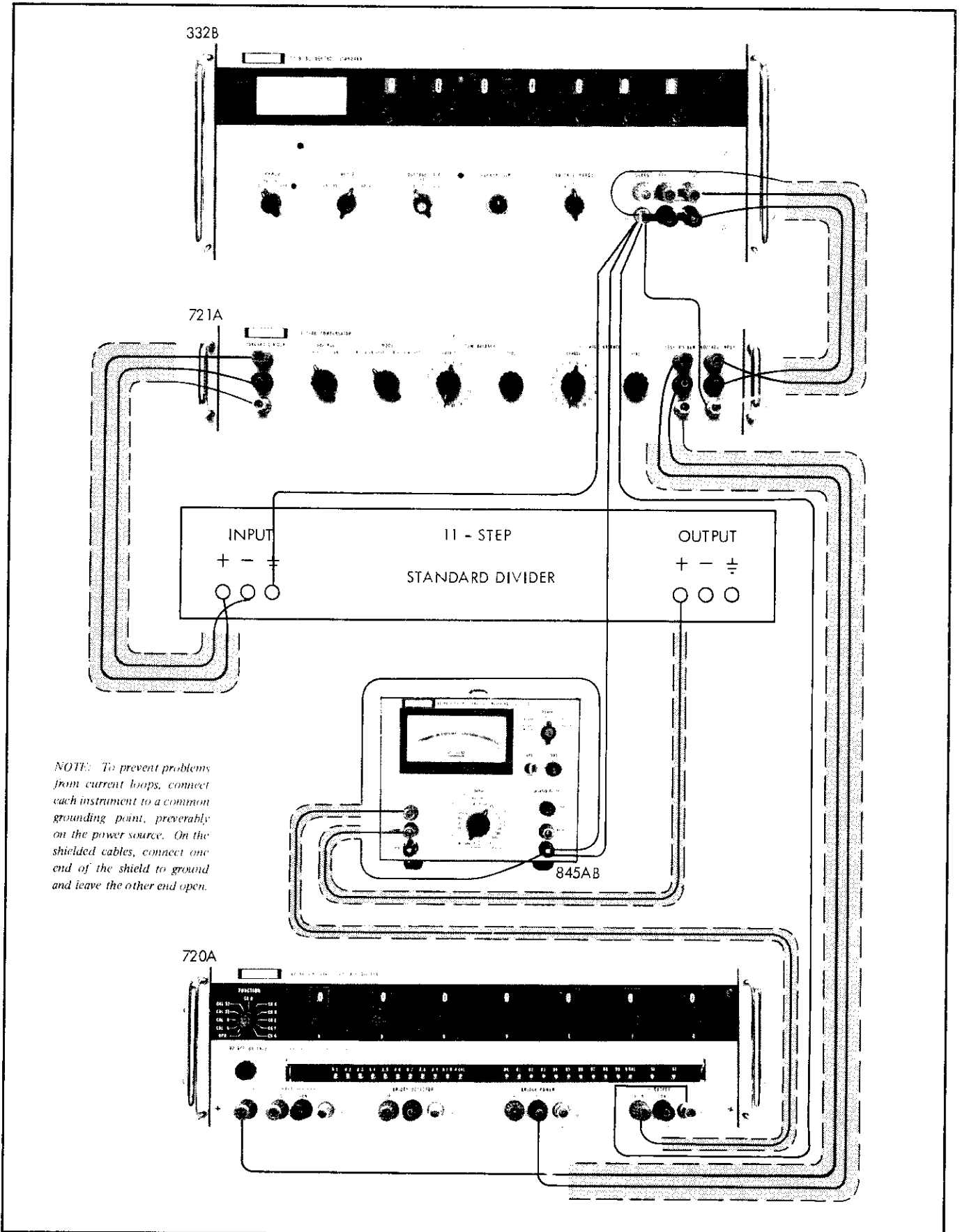


Figure 4-5. EQUIPMENT CONNECTIONS FOR DECADE LINEARITY TEST

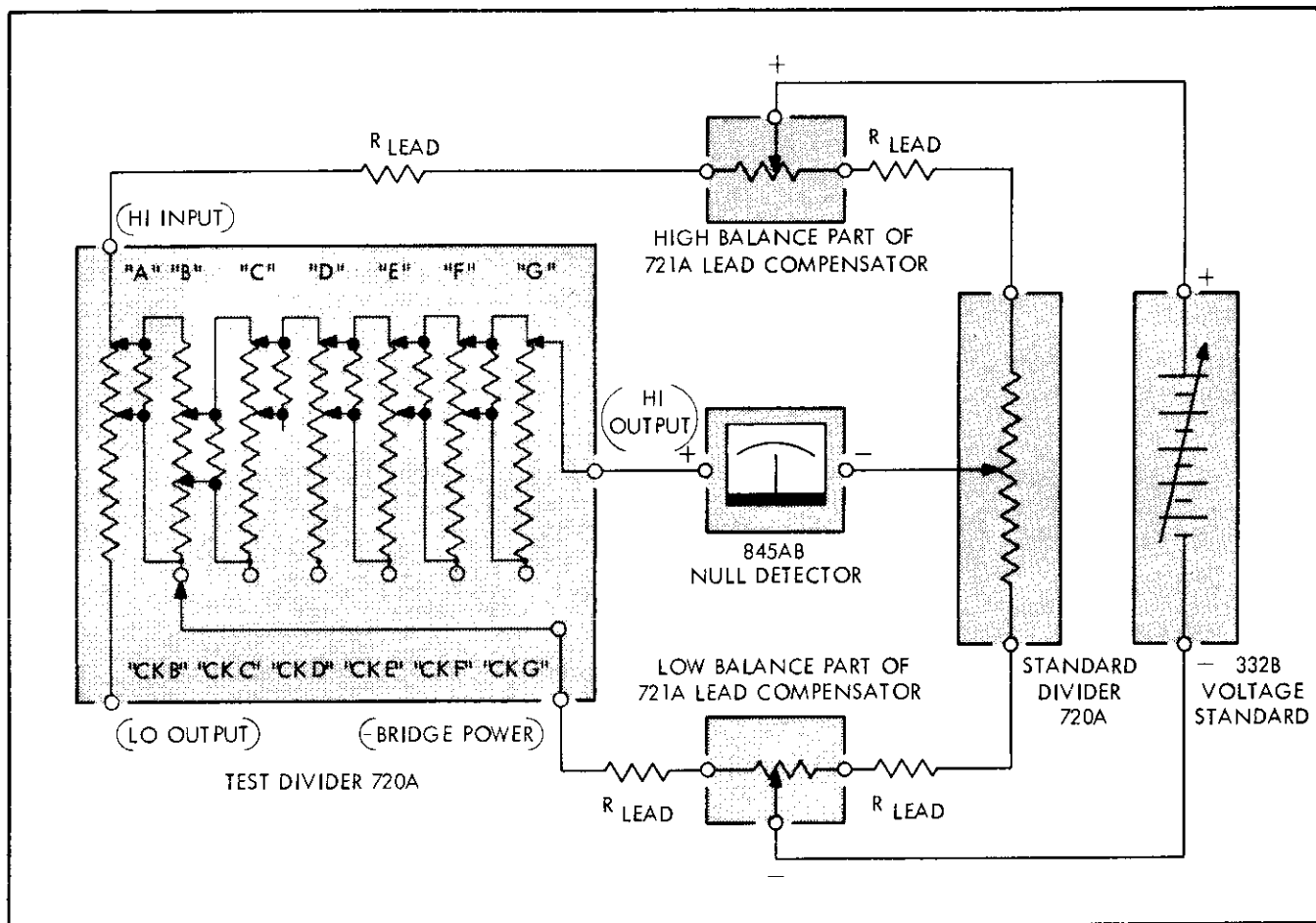


Figure 4-6. SIMPLIFIED SCHEMATIC DIAGRAM OF DECADE LINEARITY TEST

within the limits listed in the Permissible Deviation column.

NOTE!

An indication beyond these limits is a symptom of trouble within the instrument. Refer to the troubleshooting instructions to determine the nature of the fault.

- o. Set the voltage source to the desired voltage for testing the "C" decade.
- p. Turn the FUNCTION switch to CK C.
- q. Set the standard divider to zero.
- r. Set the divider under test to 1.0 900000.
- s. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- t. Adjust the LOW BALANCE CONTROLS of the lead compensator to obtain a zero indication on the null detector.
- u. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- v. Set the standard divider to full scale.
- w. Set the divider under test to 1.0 999999X.
- x. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- y. Set the divider under test back to 1.0 900000 and set the standard divider back to zero.
- z. Re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- aa. Set the null detector for the desired sensitivity and make the linearity measurements listed in Figure 4-8.
- ab. Set the voltage source to the desired test voltage for testing "D" Decade.
- ac. Turn the FUNCTION switch to CK D.

SETTINGS		PERMISSIBLE DEVIATION PPM of INPUT to "B" DECADE	MAX. TEST VOLTAGE
STANDARD DIVIDER	720A		
0	<u>1.0</u> 000000	0	100V ↓
.1	<u>1.0</u> 100000	0.38	
.2	<u>1.0</u> 200000	0.45	
.3	<u>1.0</u> 300000	0.50	
.4	<u>1.0</u> 400000	0.54	
.5	<u>1.0</u> 500000	0.57	
.6	<u>1.0</u> 600000	0.60	
.7	<u>1.0</u> 700000	0.63	
.8	<u>1.0</u> 800000	0.65	
.9	<u>1.0</u> 900000	0.67	
.999999X	<u>1.0</u> 99999X	0	
.9	<u>1.0</u> 89999X	0.67	
.8	<u>1.0</u> 79999X	0.65	
.7	<u>1.0</u> 69999X	0.63	
.6	<u>1.0</u> 59999X	0.60	
.5	<u>1.0</u> 49999X	0.57	
.4	<u>1.0</u> 39999X	0.54	
.3	<u>1.0</u> 29999X	0.50	
.2	<u>1.0</u> 19999X	0.45	
.1	<u>1.0</u> 09999X	0.38	

Figure 4-7. "B" DECADE LINEARITY TEST

- ad. Set the standard divider to zero.
- ae. Set the divider under test to 1.0 990000.
- af. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- ag. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- ah. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- ai. Set the standard divider to full scale.
- aj. Set the divider under test to 1.0 99999X.
- ak. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- al. Set the divider under test back to 1.0 990000 and set the standard divider back to zero.
- am. Re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- an. Set the null detector for the desired sensitivity and make the linearity measurements given in Figure 4-9. The null detector indications must be within the limits listed in the "permissible deviation" column.

SETTINGS		PERMISSIBLE DEVIATION PPM of INPUT to "C" DECADE	MAX. TEST VOLTAGE
STANDARD DIVIDER	720A		
0	<u>1.0</u> 900000	0	100V ↓
.1	<u>1.0</u> 910000	1.4	
.2	<u>1.0</u> 920000	1.7	
.3	<u>1.0</u> 930000	1.9	
.4	<u>1.0</u> 940000	2.1	
.5	<u>1.0</u> 950000	2.3	
.6	<u>1.0</u> 960000	2.4	
.7	<u>1.0</u> 970000	2.5	
.8	<u>1.0</u> 980000	2.7	
.9	<u>1.0</u> 990000	2.8	
.999999X	<u>1.0</u> 99999X	0	
.9	<u>1.0</u> 98999X	2.8	
.8	<u>1.0</u> 97999X	2.7	
.7	<u>1.0</u> 96999X	2.5	
.6	<u>1.0</u> 95999X	2.4	
.5	<u>1.0</u> 94999X	2.3	
.4	<u>1.0</u> 93999X	2.1	
.3	<u>1.0</u> 92999X	1.9	
.2	<u>1.0</u> 91999X	1.7	
.1	<u>1.0</u> 90999X	1.4	

Figure 4-8. "C" DECADE LINEARITY TEST

- ao. Turn the FUNCTION switch to CK E.
- ap. Set the standard divider to zero.
- aq. Set the divider under test to 1.0 999000.
- ar. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- as. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- at. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- au. Set the standard divider to full scale.
- av. Set the divider under test to 1.0 99999X.
- aw. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.
- ax. Set the divider under test back to 1.0 999000 and set the standard divider back to zero.

SETTINGS		PERMISSIBLE DEVIATION PPM of INPUT to "D" DECADE	MAX. TEST VOLTAGE
STANDARD DIVIDER	720A		
0	<u>1.0</u> 990000	0	10V ↓
.1	<u>1.0</u> 991000	6.0	
.2	<u>1.0</u> 992000	7.5	
.3	<u>1.0</u> 993000	8.6	
.4	<u>1.0</u> 994000	9.5	
.5	<u>1.0</u> 995000	10.2	
.6	<u>1.0</u> 996000	10.8	
.7	<u>1.0</u> 997000	11.4	
.8	<u>1.0</u> 998000	12.0	
.9	<u>1.0</u> 999000	12.5	
.999999X	<u>1.0</u> 99999X	0	
.9	<u>1.0</u> 99899X	12.5	
.8	<u>1.0</u> 99799X	12.0	
.7	<u>1.0</u> 99699X	11.4	
.6	<u>1.0</u> 99599X	10.8	
.5	<u>1.0</u> 99499X	10.2	
.4	<u>1.0</u> 99399X	9.5	
.3	<u>1.0</u> 99299X	8.6	
.2	<u>1.0</u> 99199X	7.5	
.1	<u>1.0</u> 99099X	6.0	

Figure 4-9. "D" DECADE LINEARITY TEST

- ay. Re-adjust the LOW BALANCE FINE control if necessary to obtain a zero indication on the null detector.
- az. Set the null detector for the desired sensitivity and make the linearity measurement given in Figure 4-10. The null detector indications must be within the limits listed in the "permissible deviation" column.
- ba. Turn the FUNCTION switch to CK F.
- bb. Set the standard divider to zero.
- bc. Set the divider under test 1.0 999900.
- bd. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- be. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- bf. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- bg. Set the standard divider to full scale.
- bh. Set the divider under test to 1.0 99999X.
- bi. Adjust the HIGH BALANCE FINE control to obtain a zero indication on the null detector.

SETTINGS		PERMISSIBLE DEVIATION PPM of INPUT to "E" DECADE	MAX. TEST VOLTAGE
STANDARD DIVIDER	720A		
0	<u>1.0</u> 999000	0	10V ↓
.1	<u>1.0</u> 999100	28	
.2	<u>1.0</u> 999200	35	
.3	<u>1.0</u> 999300	40	
.4	<u>1.0</u> 999400	44	
.5	<u>1.0</u> 999500	47	
.6	<u>1.0</u> 999600	50	
.7	<u>1.0</u> 999700	53	
.8	<u>1.0</u> 999800	55	
.9	<u>1.0</u> 999900	57	
.999999X	<u>1.0</u> 999990	0	
.9	<u>1.0</u> 99989X	57	
.8	<u>1.0</u> 99979X	55	
.7	<u>1.0</u> 99969X	53	
.6	<u>1.0</u> 99959X	50	
.5	<u>1.0</u> 99949X	47	
.4	<u>1.0</u> 99939X	44	
.3	<u>1.0</u> 99929X	40	
.2	<u>1.0</u> 99919X	35	
.1	<u>1.0</u> 99909X	28	

Figure 4-10. "E" DECADE LINEARITY TEST

- bj. Set the divider under test back to 1.0 999900 and set the standard divider back to zero.
- bk. Re-adjust the LOW BALANCE FINE control if necessary to obtain zero indication on the null detector.
- bl. Set the null detector for the desired sensitivity and make the linearity measurements given in Figure 4-11. The null detector indications must be within the limits listed in the "permissible deviation" column.
- bm. Turn the FUNCTION switch to CK G.
- bn. Set the standard divider to zero.
- bo. Set the divider under test to 1.0 999990.
- bp. Place the null detector in the zero mode, adjust it for zero deflection, and return it to operating mode.
- bq. Adjust the LOW BALANCE controls of the lead compensator to obtain a zero indication on the null detector.
- br. Turn the HIGH BALANCE COARSE control to the same setting as the LOW BALANCE COARSE control.
- bs. Set the standard divider to full scale.
- bt. Set the divider under test to 1.0 99999X.

SETTINGS		PERMISSIBLE DEVIATION PPM of INPUT to "F" DECADE	MAX. TEST VOLTAGE
STANDARD DIVIDER	720A		
0	<u>1.0</u> 999900	0	10V ↓
.1	<u>1.0</u> 999910	130	
.2	<u>1.0</u> 999920	160	
.3	<u>1.0</u> 999930	180	
.4	<u>1.0</u> 999940	200	
.5	<u>1.0</u> 999950	220	
.6	<u>1.0</u> 999960	230	
.7	<u>1.0</u> 999970	240	
.8	<u>1.0</u> 999980	260	
.9	<u>1.0</u> 999990	270	
.999999X	<u>1.0</u> 99999X	0	
.9	<u>1.0</u> 99998X	270	
.8	<u>1.0</u> 99997X	260	
.7	<u>1.0</u> 99996X	240	
.6	<u>1.0</u> 99995X	230	
.5	<u>1.0</u> 99994X	220	
.4	<u>1.0</u> 99993X	200	
.3	<u>1.0</u> 99992X	180	
.2	<u>1.0</u> 99991X	160	
.1	<u>1.0</u> 99990X	130	

Figure 4-11. "F" DECADE LINEARITY TEST

- bu. Adjust the **HIGH BALANCE FINE** control to obtain a zero indication on the null detector.
- bv. Set the divider under test back to 1.0 999990 and set the standard divider back to zero.
- bw. Re-adjust the **LOW BALANCE FINE** control if necessary to obtain a zero indication on the null detector.
- bx. Set the null detector for the desired sensitivity and make the linearity measurements given in Figure 4-12. The null detector indications must be within the limits listed in the "permissible deviation" column.
- by. Disconnect the test equipment and return the FUNC-

TION switch to OPR position; the decade linearity tests are complete.

4-19. CALIBRATION

4-20. Calibration of the Model 720A consists of calibrating two standard resistance arms of the internal Wheatstone bridge and calibrating the first three decades. The bridge arms require calibration only if the **BRIDGE BALANCE** control has insufficient range to balance the bridge during divider calibration.

4-21. Divider Calibration

4-22. This procedure is used to adjust the linearity of the "A", "B" and "C" decades of the Model 720A so

SETTINGS		PERMISSIBLE DEVIATION PPM of INPUT to "G" DECADE	MAX. TEST VOLTAGE
STANDARD DIVIDER	720A		
0	1.0 999990	0	10V ↓
.1	1.0 999991	600	
.2	1.0 999992	750	
.3	1.0 999993	860	
.4	1.0 999994	950	
.5	1.0 999995	1020	
.6	1.0 999996	1080	
.7	1.0 999997	1140	
.8	1.0 999998	1200	
.9	1.0 999999	1250	
.999999X	1.0 99999X	0	

Figure 4-12. "G" DECADE LINEARITY TEST

that any readout setting is accurate within 0.1 ppm of input. This procedure consists of two parts, calibration of the "C" decade and the "S3" shunt, and calibration of the "A" and "B" decades, and their shunts. The latter is the self calibration procedure which is performed from the front panel.

4-23. To calibrate the "C" decade and "S3" shunt proceed as follows:

NOTE!

SEE NOTE ON PG. 4-18 CONCERNING R205

Insure the system has the correct connections and ground as shown in Figure 4-14.

- Turn the FUNCTION switch to OPR, turn the internal FUNCTION switch to CAL C, exercise the "C" decade switch by turning it twice through all positions, and set the readout to .000000.
- Connect the voltage source to the red and the black BRIDGE POWER binding posts.
- Connect the null detector to the BRIDGE DETECTOR binding posts. The guard terminal of the null detector must be connected to the common terminal.

- Turn the B decade switch to the blank position and apply 10 volts from the voltage source.
- Adjust the BRIDGE BALANCE control to obtain a null indication ± 10 microvolts.

NOTE!

If the null meter cannot be nulled using the Bridge Balance Control, perform the Bridge Calibration Procedure (paragraph 4-25).

- Locate the C-0 trimmer (R1130) on the circuit board and sweep it slowly from stop to stop while observing the null detector. If the indication does not change smoothly, sweep it from stop to stop several times.
- Set the null detector to the 30 microvolt range and adjust the C-0 trimmer to obtain an indication of 0 ± 10 microvolts.
- Observe the null detector and tap the trimmer; the indication should remain within 10 microvolts of zero.

- i. Use the following procedure to calibrate the "C" deck switch positions 1 through CAL:
1. Turn the "C" deck switch clockwise to the next position to be calibrated.
 2. Observe the null detector and slowly sweep the trimmer corresponding to the switch position (C-1 through C CAL) from stop to stop. If the indication does not change smoothly, sweep the trimmer from stop to stop several times.
 3. Observe the null detector and adjust the trimmer to obtain an indication of 0 ± 10 microvolts.
 4. Observe the null detector and tap the trimmer; the indication should stay within 10 microvolts of the zero.
 5. Turn the "C" deck switch away from the position being calibrated, return it and observe the meter. The indication should be within 10 microvolts of zero
- o. Turn the "C" decade switch away from the 0 positions and return it to zero. The null detector indication should be within 10 microvolts of zero.
- p. Return the internal FUNCTION switch to OPR; Calibration of the "C" decade and S3 shunt is complete.
- 4-24. To calibrate the "A" and "B" decades, perform the self-calibration procedure using the instructions given in paragraphs 2-24 and 2-25.

4-25. Bridge Calibration

NOTE!

The Bridge Calibration procedure is required only if a null could not be obtained during Divider Calibration with the BRIDGE BALANCE Control.

4-26. 10-KILOHM BRIDGE STANDARD. This procedure is used to adjust the total resistance of the bridge arm used for calibration of the "A" and "B" decades (self-calibration of the instrument) so the bridge can be balanced to measure a nominal 10,000 ohms. If the bridge can be balanced near the center of travel for the BRIDGE BALANCE during self-cal at CAL A - Zero positions the procedure following does not need to be performed. However, if during self-cal in the CAL A - Zero position (See paragraph 2-24) the bridge cannot be balanced using the BRIDGE BALANCE Control, perform the procedure below:

NOTE!

Insure the system has the correct connections and ground as shown in Figure 4-14.

6. Proceed to the next position to be calibrated.
- j. Return the "C" deck switch to the 0 position.
- k. Turn the internal FUNCTION switch to the CAL S3 position.
- l. Observe the null detector and slowly sweep the CAL S3 trimmer from stop to stop. If the indication does not change smoothly, sweep it from stop to stop several times.
- m. Adjust the CAL S3 trimmer to obtain an indication of 0 ± 10 microvolts.
- n. Observe the null detector and tap the trimmer. The indication should stay within 10 microvolts of zero.
- a. Turn the FUNCTION switch to CAL A; turn the internal FUNCTION switch to OPR (Fig. 4-13) and set the readout to .0000000.
- b. Connect a 20 volt DC source to the red and the black BRIDGE POWER binding posts.
- c. Connect the null detector to the BRIDGE DETECTOR binding posts. The guard terminal of the null detector must be connected to the Common terminal.

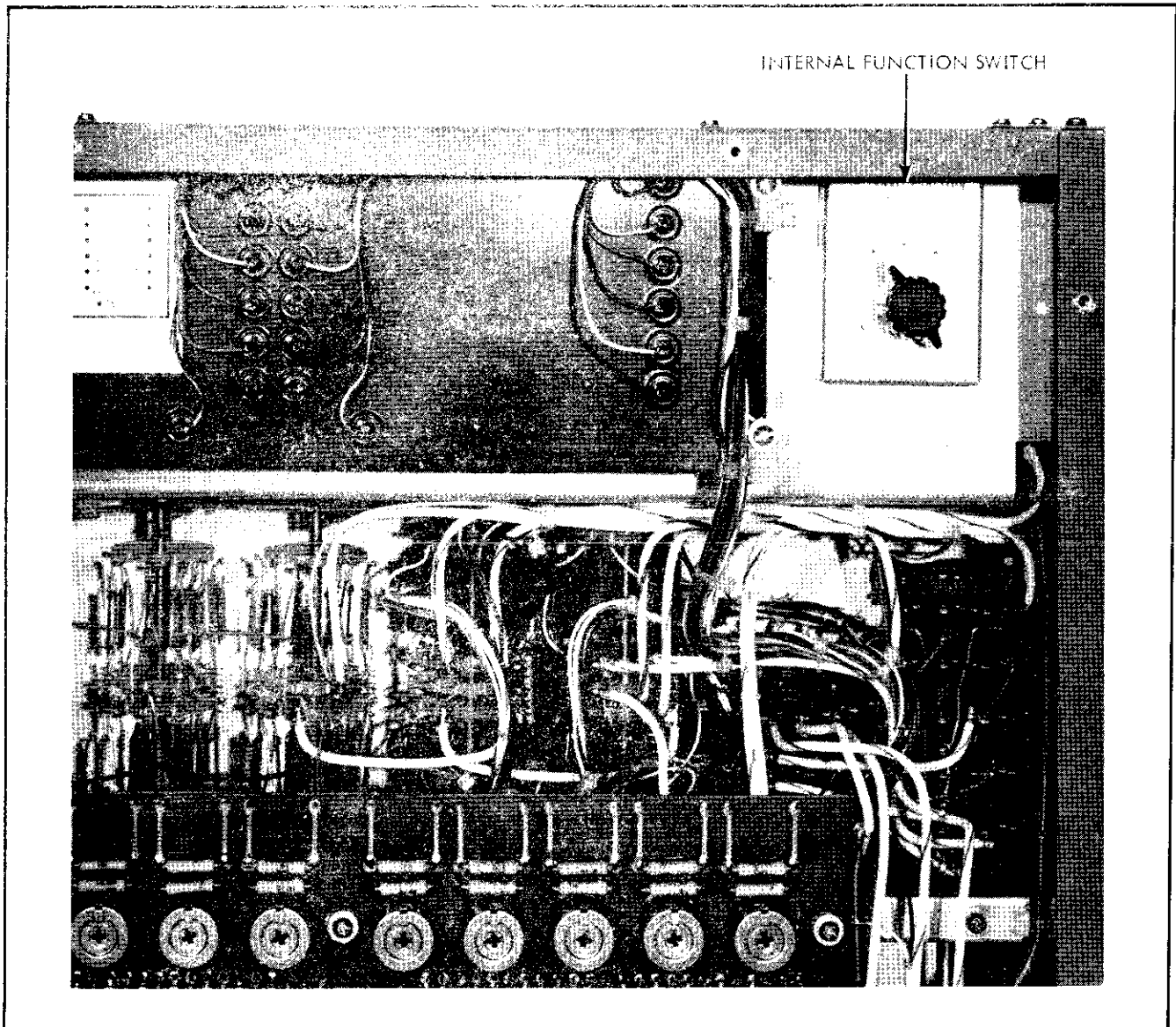


Figure 4-15. INTERNAL FUNCTION SWITCH

- d. Adjust the Bridge Balance control to the center of its travel range.

NOTE:

BRIDGE BALANCE is a potentiometer control with both a Fine and Coarse range on the same control knob.

- e. Observe the null detector scale. Rotate the bridge element beneath the null detector until the indication reads a change of 100 microvolts. Rotate R203 from stop to stop several times.
- f. Adjust R203 to obtain an indication of 0 \pm 100

microvolts.

- g. Select the one millivolt range on the null detector. Vary the Bridge Balance control while observing the null detector. When the electrical center is obtained, leave the BRIDGE BALANCE control at that position.
- h. Re-adjust R203 to obtain an indication of 0 \pm 100 microvolts.
- i. Calibration of the 10-kilohm bridge standard is complete.

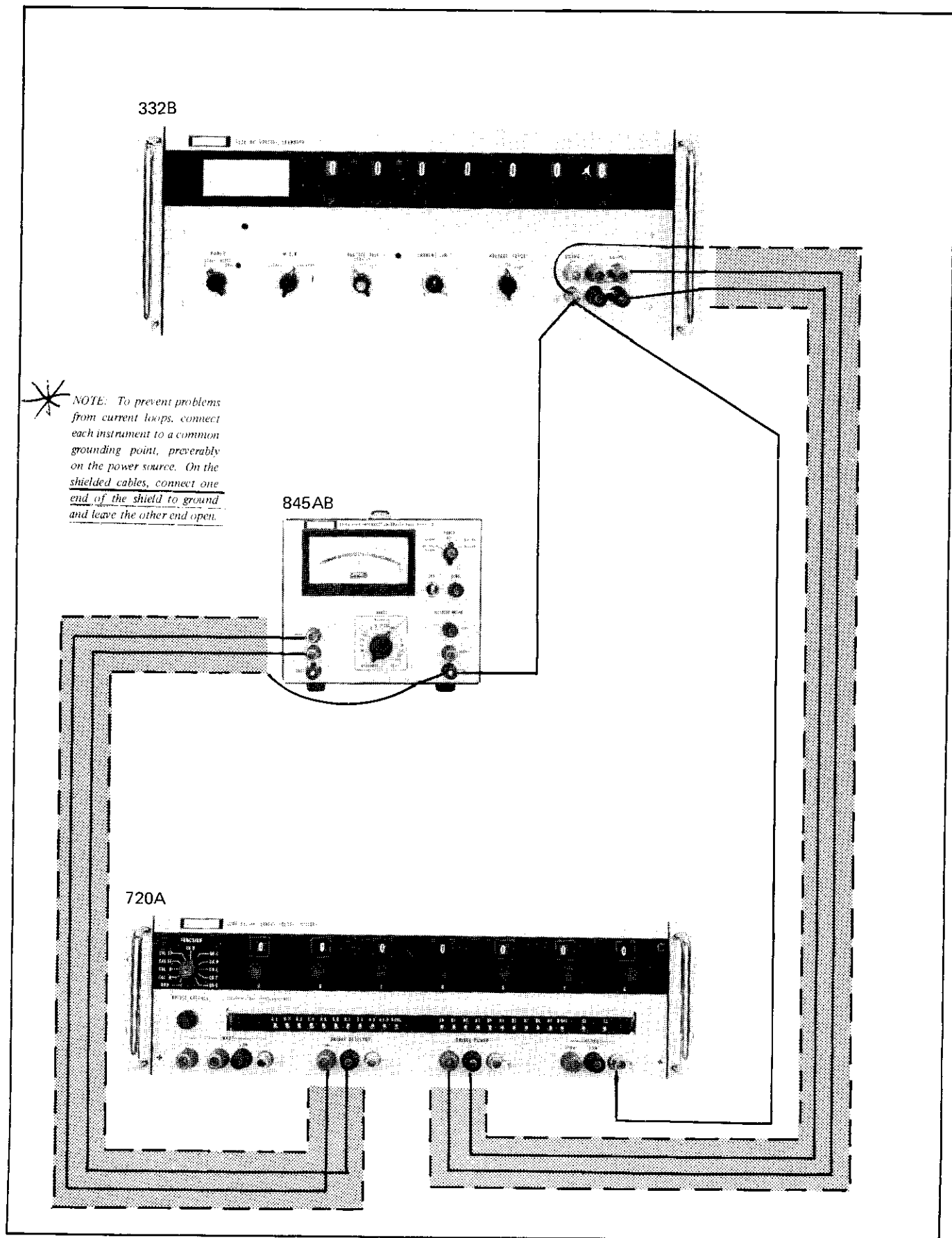


Figure 4-14. EQUIPMENT CONNECTIONS FOR SELF CALIBRATION.

NOTE!

The BRIDGE BALANCE control and R203 are now ready for the self-cal procedures for A and B decades in paragraph 2-24, assuming R312 and its associated trim resistors have not shifted excessively in value. If insufficient trim range remains at A.1, A.2, etc., the 720A should be returned to the factory for repair. Perform the C decade and S3 shunt check in paragraph 4-21 prior to performing the self-cal at A and B decades.

4-27. 4-KILOHM BRIDGE STANDARD. This procedure is used to adjust the total resistance of the bridge arm used for calibration of the third "C" decade so the bridge can be balanced to measure a nominal 4007.6 ohms. Calibration of the "C" decade consists of setting each step on the decade to a nominal 4007.6 ohms. If the bridge can be balanced with the BRIDGE BALANCE control on the front panel during self-cal in the CAL C - Zero position described in paragraph 4-21, this procedure does not need to be performed. To reset the range of the BRIDGE BALANCE control for balance of the bridge, perform the following procedure:

- a. Turn the FUNCTION switch to OPR, and turn the internal FUNCTION switch to CAL C, and set the readout to .0000000.

NOTE!

The internal FUNCTION switch, which is shown in Figure 4-13, is used only for calibration of the "C" decade and the S-3 shunt. It should not be confused with the FUNCTION switch located on the front panel.

- b. Connect the voltage source to the red and the black BRIDGE POWER binding posts.
- c. Connect the null detector to the BRIDGE DETECTOR binding posts. The guard terminal of the null detector must be connected to the common terminal.
- d. Turn the ^{"B"}~~"C"~~ decade switch to the blank position and apply 10 volts from the voltage source.
- e. Adjust BRIDGE BALANCE to the mid-position and adjust R1130 (Decade C-9) to mid position

- f. Observing the Null Detector sweep R205 (Bridge Circuit Board) thru its range. If the null detector does not show a smooth change, sweep R205 through its range several times.
- g. Adjust R205 for 0 ± 50 microvolts on the Null Detector.
- h. Place the Null Detector on the 300 microvolt range. Observe the range of the BRIDGE BALANCE control on the Null Detector and place the BRIDGE BALANCE control at the electrical center.
- i. Adjust R1130 (Decade C-0) for 0 ± 10 microvolts.

NOTE!

The BRIDGE BALANCE control, R205 and R1130 are now set to give a nominal 4007.6 ohm reference and the self-cal procedure in paragraph 4-21 will make the other positions of the C Decade the same value. If there is not enough range to trim the remaining positions of the C Decade to this nominal value repeat steps a through i with different settings for R205 and R1130. If calibration still is not possible, return the 720A to the factory for repair.

- j. Disconnect the test equipment; calibration of the 4-kilohm bridge standard is complete.

4-28. TROUBLESHOOTING

4-29. Troubles in the Model 720A may be located most easily by performing the decade linearity test described in paragraph 4-15 and analyzing the results. Reference to the schematic diagram will greatly assist in the analysis. Before attempting to locate the trouble, the instrument should first be cleaned following the procedure described in paragraph 4-10 and the leakage resistance should be measured following the procedure described in paragraph 4-8.

4-30. Because of the passive nature of the instrument, troubles will be limited to defective resistors, defective switches, defective wiring, and excessive leakage will usually be corrected by cleaning. If repeated cleaning fails to correct the condition, the instrument should be returned to the factory for repair.

4-31. Not only may resistor defects be isolated to a particular step of a decade by the linearity test, but also the nature of the defect may be determined. A resistor may be shorted, open, over value, or under value. Because the switch contacts span two steps of resistance in all decades except the seventh ("G"), the

effect caused directly by a defective resistor will be seen at two adjacent switch positions. In the "D" through "G" decades the linearity test will isolate the defect to a particular resistor. In the "A", "B", and "C", decades each step is made up of several resistors and each resistor in the step will have to be measured to find the defect. In these decades, the variable trimmer resistor in the defective step should be checked by monitoring it and sweeping it from stop to stop several times. If the variation is not smooth, it should be replaced. If one of the resistors in the oil tank or one of the factory selected fixed resistors is found to be defective, the instrument should be returned to the factory for repair.

4-32. A shorted resistor will decrease the overall resistance of the decade thereby increasing the proportional value of all steps except the one containing the shorted resistor. The proportional value of this step will be very low.

4-33. An open resistor in any decade will prevent any output until the switch is advanced so the contacts span the open resistor. At this point the ratio will be high. As the switch is advanced so the contacts no longer span the open resistor, the measured output will be the source voltage. If a decade shunt is open all steps of the decade will be equal but resistance of the decade will be high. This will cause nonlinearity in the preceding decade which may be observed by dialing it upward from zero. Below the midpoint, the output will be high; above the midpoint, the output will be low.

4-34. An over value resistor in any decade will reduce the proportion of all other steps and increase the proportion of the step containing the over value resistor. In all decades except the seventh, this increase will be seen at two adjacent switch positions because the switch contacts span two resistance steps. In the seventh decade, there will be only one over value step. If a decade shunt is over value, all steps of the decade will be equal but the resistance of the decade will be high. This will cause nonlinearity in the preceding decade which may be observed by dialing it upward from zero. Below the midpoint, the output will be high; above the midpoint, the output will be low.

4-35. An under value resistor in any decade will increase the proportion of all other steps and decrease the proportion of the step containing the under value resistor. In all decades except the seventh, this decrease will be seen at two adjacent switch positions. In the seventh decade there will be only one under value step. If a decade shunt is under value, all steps of the decade will be equal but the resistance of the decade will be low. This will cause nonlinearity in the preceding decade which may be observed by dialing it upward from zero. Below the midpoint, the output will be low; above the midpoint, the output will be high.

4-36. A defective switch usually will cause erratic or irregular operation of the decade. A broken contact may cause one step to be missing although all others are of the correct value or it may completely open the divider circuit. When a switch defect is suspected, the switch should be checked for continuity at each position.

4-37. Defective wiring usually will cause one step of a decade to be missing or will completely open the divider circuit. Wiring continuity should be checked to isolate the fault.

4-38. REPAIR

4-39. Any parts of the Model 720A except factory selected resistors and resistors housed in the oil tank may be replaced without difficulty by an experienced electronic maintenance technician. When a switch is replaced all leads should be tagged as they are disconnected to assure that they are correctly connected to the new switch. Care should be exercised in any soldering operation to assure that good electrical contact is made. All parts except precision wirewound resistors may be ordered from the factory by giving only the information specified in paragraph 5-4.

4-40. The precision wirewound resistors used in the Model 720A are selected and matched during manufacture to form a completely matched set. Sufficient information is marked on each of these resistors to permit replacement with a resistor which will match the others in the set. The following information should be given when one of these resistors is ordered from the factory:

- a. Serial number of the instrument.
- b. Reference designation of the resistor.
- c. All markings on the resistor.

If all markings on the defective resistor can not be read, give the following information:

- a. Serial number of the instrument.
- b. Reference designation of the defective resistor.
- c. Reference designation and all part markings of the adjacent resistor on one side.
- d. Reference designation and all part markings of the adjacent resistor on the other side.

4-41. SERVICE INFORMATION

4-42. The John Fluke Manufacturing Co., Inc. warrants each instrument manufactured by them for the period of one year upon making delivery of the instrument to you, the original purchaser. Complete warranty page located at the rear of this manual.

4-43. If you should encounter any problem in the operation of your instrument, please feel free to contact your nearest John Fluke Sales Representative or write directly to the John Fluke Manufacturing Co., Inc. with a statement of your problem.

Section 5

List of Replaceable Parts

5-1. INTRODUCTION

5-2. This section contains complete descriptions of those parts one might normally expect to replace during the life of the instrument. The first listing is a breakdown of all of the major assemblies in the instrument. Subsequent listings itemize the components in each assembly. Every listing is accompanied by an illustration identifying each component in the listing. Assemblies and subassemblies are identified by name in the parts list and by a ten digit stock number in the illustrations. Components are identified by the schematic diagram reference designation (e.g. R1, C107 DS1). Parts not appearing on the schematic diagram are numbered consecutively throughout the parts list with a whole number. Flagnotes are used throughout the parts list and refer to ordering explanations. The flagnote explanations appear at the end of the parts list in which they are listed.

5-3. COLUMNAR INFORMATION

- a. The REF DESIG column indexes the item description to the associated illustration. In general the reference designations are listed under each assembly in alpha-numeric order. Subassemblies of minor proportions are sometimes listed with the assembly of which they are a part. In this case, the reference designations for the components of the subassembly may appear out of order.
- b. The DESCRIPTION column describes the salient characteristics of the component. Indentation of the description indicates the relationship to other assemblies, components, etc. In many cases it is necessary to abbreviate in this column. For abbreviations and symbols used, see the following page.
- c. The ten-digit part number by which the item is identified at the John Fluke Mfg. Co. is listed in the STOCK NO. column. Use this number when ordering parts from the factory or authorized representatives.
- d. The Federal Supply Code for the item manufacturer is listed in the MFR column. An abbreviated list of Federal Supply Codes is included in the Appendix.
- e. The part number which uniquely identifies the item to the original manufacturer is listed in the MFR PART NO column. If a component must be ordered by description, the type number is listed.
- f. The TOT QTY column lists the total quantity of the item used in the instrument. Second and subsequent listing of the same item are referenced to the first listing with the abbreviation REF. In the case of optional subassemblies, plug ins, etc. that are not always part of the instrument, the TOT QTY column lists the total quantity of the item in that particular assembly.
- g. Entries in the REC QTY column indicate the recommended number of spare parts necessary to support one to five instruments for a period of two years. This list presumes an availability of common electronic parts at the maintenance site. For maintenance for one year or more at an isolated site, it is recommended that at least one of every part in the instrument be stocked.
- h. The USE CODE column identifies certain parts which have been added, deleted or modified during the production of the instrument. Each part for which a Use Code has been assigned may be identified with a particular instrument serial number by consulting the Serial Number Effectivity List. As Use Codes are added to the list, the TOT QTY column listings are changed to reflect the most current information. Sometimes when a part is changed, the new part can and should be used as a replacement for the original part. In this event a parenthetical note is added in the DESCRIPTION column.

5-4. HOW TO OBTAIN PARTS

5-5. Standard components have been used wherever possible. Standard components may be ordered directly from the manufacturer by using the manufacturer's part number, or parts may be ordered from the John Fluke Mfg. Co. factory or authorized representative by using the Fluke part number. In the event the part you order has been replaced by a new or improved part, the replacement will be accompanied by an explanatory note and installation instructions, if necessary.

5-6. You can insure prompt and efficient handling of your order to the John Fluke Mfg. Co. if you include the following information:

- a. Quantity.
- b. FLUKE Stock Number.
- c. Description.
- d. Reference Designation.
- e. Instrument model and serial number.

Example; 2 each, 4805-177105, Transistors, 2N3565, Q107-108 for 845AR, s/n 168.

If you must order structural parts not listed in the parts list, describe the part as completely as possible. A sketch of the part showing its location to other parts of the instrument is usually most helpful.

5-8. SERIAL NUMBER EFFECTIVITY

5-9. A Use Code column is provided to identify certain parts that have been added, deleted, or modified during production of the Model 720A. Each part for which a use code has been assigned may be identified with a particular instrument serial number by consulting the Use Code Effectivity List below. All parts with no code are used on all instruments with serial numbers above 123. New codes will be added as required by instrument changes.

USE CODE	EFFECTIVITY
No Code	Model 720A, serial number 123 and on.
A	Model 720A, serial number 536 and on.

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
	KELVIN-VARLEY VOLTAGE DIVIDER Figure 5-1	720A					
	Front Panel Assembly (See Figure 5-2)						
	Trimmer P/C Assembly (See Figure 5-3)	1702-210716 (720A-4001)	89536	1702-210716	1		
	Bridge P/C Assembly (See Figure 5-4)	1702-200295 (720A-4002)	89536	1702-200295	1		
	Resistor Can Assembly If a resistor in this assembly requires replacement, the entire instrument must be returned to the factory for repair and recalibration.	3158-217612 (720A-4018)	89536	3158-217612	1		
S1	Switch, "A" DECADE, rotary, 3p, 12 pos, 3 sect	5105-220012	89536	5105-220012	1		
	"B" Decade Switch Assembly (See Figure 5-5)	5110-217307 (720A-4004)	89536	5110-217307	1		
	"C" Decade Switch Assembly (See Figure 5-6)	5110-217315 (720A-4005)	89536	5110-217315	1		
	"D", "E", "F" and "G" Decades Switch Assy. (See Figure 5-7)	5110-217323 (720A-4006)	89536	5110-217323	1		
S8	Switch, FUNCTION, 5p, 11 pos, 5 sect	5105-220020	89536	5105-220020	1		
S9	Switch, INTERNAL FUNCTION, 4p, 3 pos, 2 sect	5107-218560	89536	5107-218560	1		
1	Bushing, dial	2502-130435	89536	2502-130435	7		
1	Bushing, dial	3153-130252	89536	3153-130252	7		A
2	Coupler, switch (not illustrated)	2402-200592	89536	2402-200592	7		
3	Cover, bottom (not illustrated)	3156-217117	89536	3156-217117	1		
4	Cover, internal function switch	3156-217521	89536	3156-217521	1		
5	Cover, top (not illustrated)	3156-217125	89536	3156-217125	1		
6	Detent, switch	5108-218578	89536	5108-218578	6		
7	Detent, internal function switch (not illustrated)	5108-218552	89536	5108-218552	1		
8	Dial, 0.0 - 1.0 Cal	2403-208611	89536	2403-208611	1		
9	Dial, 0 - Cal	2403-208595	89536	2403-208595	2		
10	Dial, 0 - X	2403-208603	89536	2403-208603	1		
11	Dial, 0 - 9	2403-208587	89536	2403-208587	3		
12	Foot, rubber (not illustrated)	2819-103309	77969	9102-W	4		
13	Heat sink, resistor	3156-217463	89536	3156-217463	1		
14	Knob, INTERNAL FUNCTION	2405-170050	89536	2405-170050	1		
15	Panel, rear	3156-217075	89536	3156-217075	1		

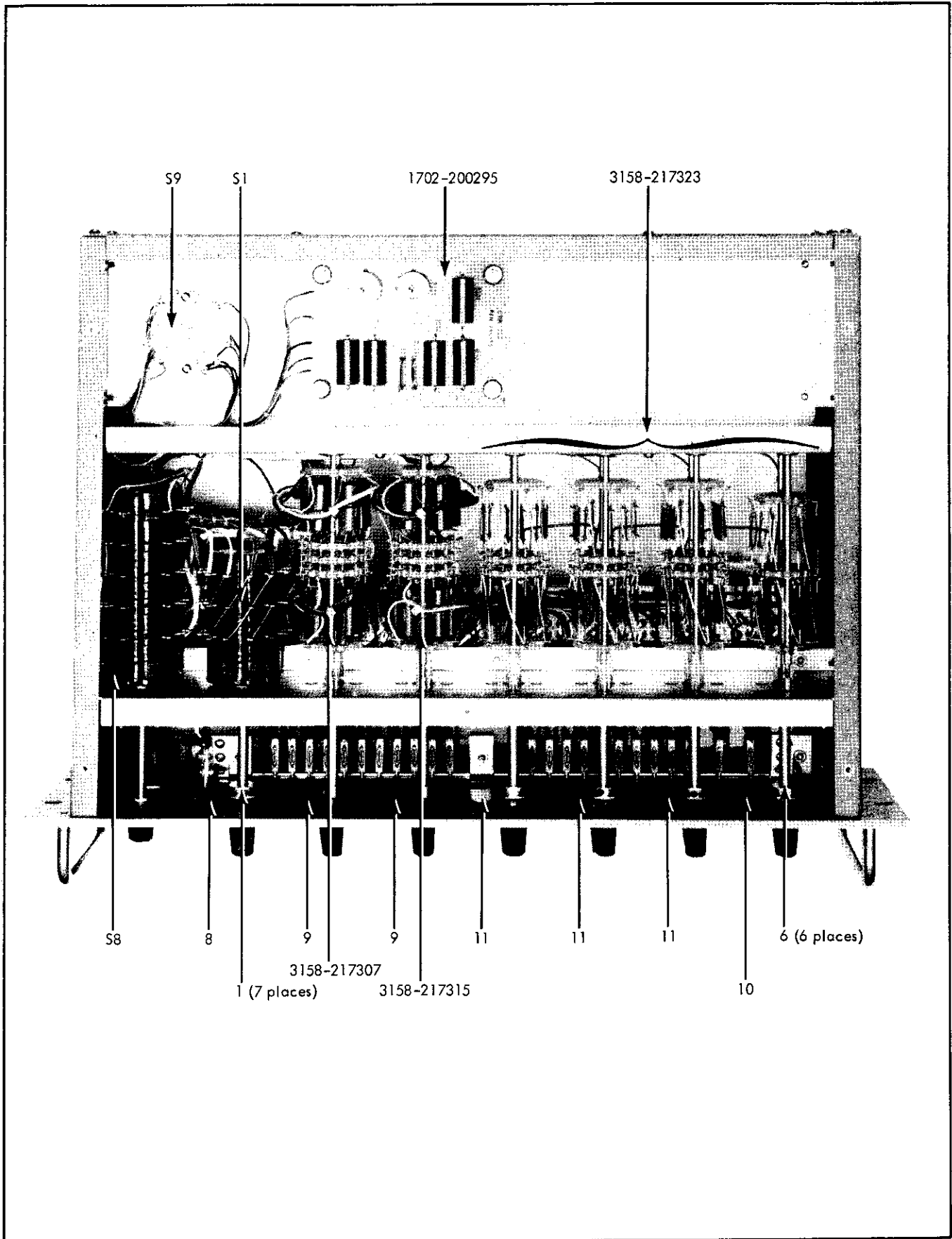


Figure 5-1. 720A KELVIN-VARLEY VOLTAGE DIVIDER (Sheet 1 of 2)

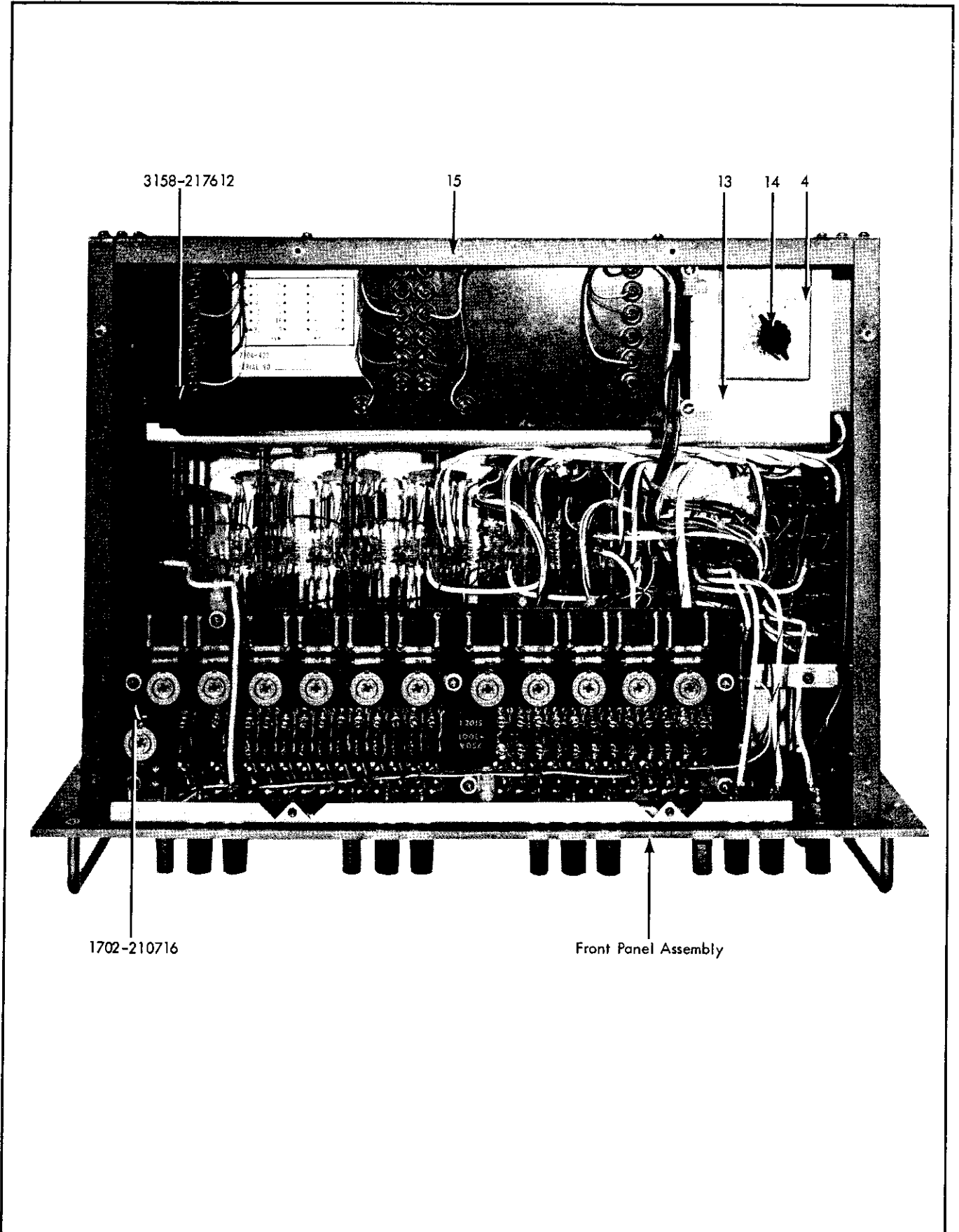


Figure 5-1. 720A KELVIN-VARLEY VOLTAGE DIVIDER (Sheet 2 of 2)

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
FRONT PANEL ASSEMBLY - Figure 5-2							
J1	Binding post, red, 1.1 INPUT	2811-149856	58474	BHB-10208-G22	5		
J2	Binding post, red, 1.0 INPUT	2811-149856	58474	BHB-10208-G22	REF		
J3	Binding post, black, LOW INPUT	2811-149864	58474	BHB-10208-G21	4		
J4	Binding post, GROUND INPUT	2811-155911	58474	GP30NC	4		
J5	Binding post, red, HIGH OUTPUT	2811-149856	58474	BHB-10208-G22	REF		
J6	Binding post, black, LOW OUTPUT	2811-149864	58474	BHB-10208-G21	REF		
J7	Binding post, GROUND OUTPUT	2811-155911	58474	GP30NC	REF		
J8	Binding post, black, - BRIDGE DETECTOR	2811-149864	58474	BHB-10208-G21	REF		
J9	Binding post, red, + BRIDGE DETECTOR	2811-149856	58474	BHB-10208-G22	REF		
J10	Binding post, GROUND BRIDGE DETECTOR	2811-155911	58474	GP30NC	REF		
J11	Binding post, red, + BRIDGE POWER	2811-149856	58474	BHB-10208-G22	REF		
J12	Binding post, black, - BRIDGE POWER	2811-149864	58474	BHB-10208-G21	REF		
J13	Binding post, GROUND BRIDGE POWER	2811-155911	58474	GP30NC	REF		
R1	Res, var, ww, 5k \pm 3%, 3w, BRIDGE BALANCE (not illustrated)	4702-215319	89536	4702-215319	1		
16	Cover, calibration access	3156-217083	89536	3156-217083	1		
17	Handle, chrome-plated brass	2404-101683	15849	1010-13	2		
18	Knob, A through G	2405-158949	89536	2405-158949	7		
19	Knob, BRIDGE BALANCE	2405-158956	89536	2405-158956	1		
20	Knob, FUNCTION	2405-190249	89536	2405-190249	1		
21	Panel, front	1406-217042	89536	1406-217042	1		

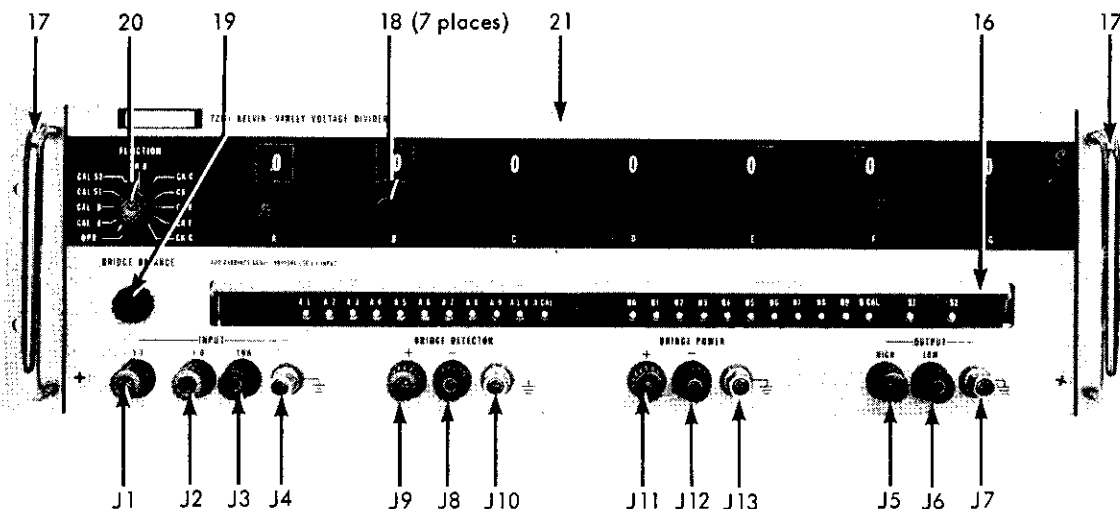















Figure 5-2. FRONT PANEL ASSEMBLY

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
	TRIMMER P/C ASSEMBLY -Figure 5-3	1702-210716 (720A-4001)	89536	1702-210716	REF		
R1001	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	24		
R1002	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	12		
R1003	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	23	1	
R1004	Res, ww, factory selected						
R1005	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1006	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	REF		
R1007	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1008	Res, ww, factory selected						
R1009	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1010	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4702-159475	12400	Type CEC-TO	REF		
R1011	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1012	Res, ww, factory selected						
R1013	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1014	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	REF		
R1015	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1016	Res, ww, factory selected						
R1017	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1018	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	REF		
R1019	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1020	Res, ww, factory selected						
R1021	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1022	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	REF		
R1023	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1024	Res, ww, factory selected						
R1025	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1026	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	REF		
R1027	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1028	Res, ww, factory selected						
R1029	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1030	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	REF		
R1031	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1032	Res, ww, factory selected						
R1033	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1034	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	REF		
R1035	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1036	Res, ww, factory selected						
R1037	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1038	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	REF		
R1039	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1040	Res, ww, factory selected						
R1041	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		
R1042	Res, met flm, 8.45k $\pm 1\%$, 1/2w	4705-159475	12400	Type CEC-TO	REF		
R1043	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1044	Res, ww, factory selected						
R1045	Res, ww, 100 Ω $\pm 0.5\%$, 1/2w	4707-155846	89536	4707-155846	REF		
R1046	Res, ww, factory selected						
R1047	Res, ww, factory selected						
R1048	Res, var, ww, 5k $\pm 10\%$, 1w	4702-215269	02660	3800P-502	REF		

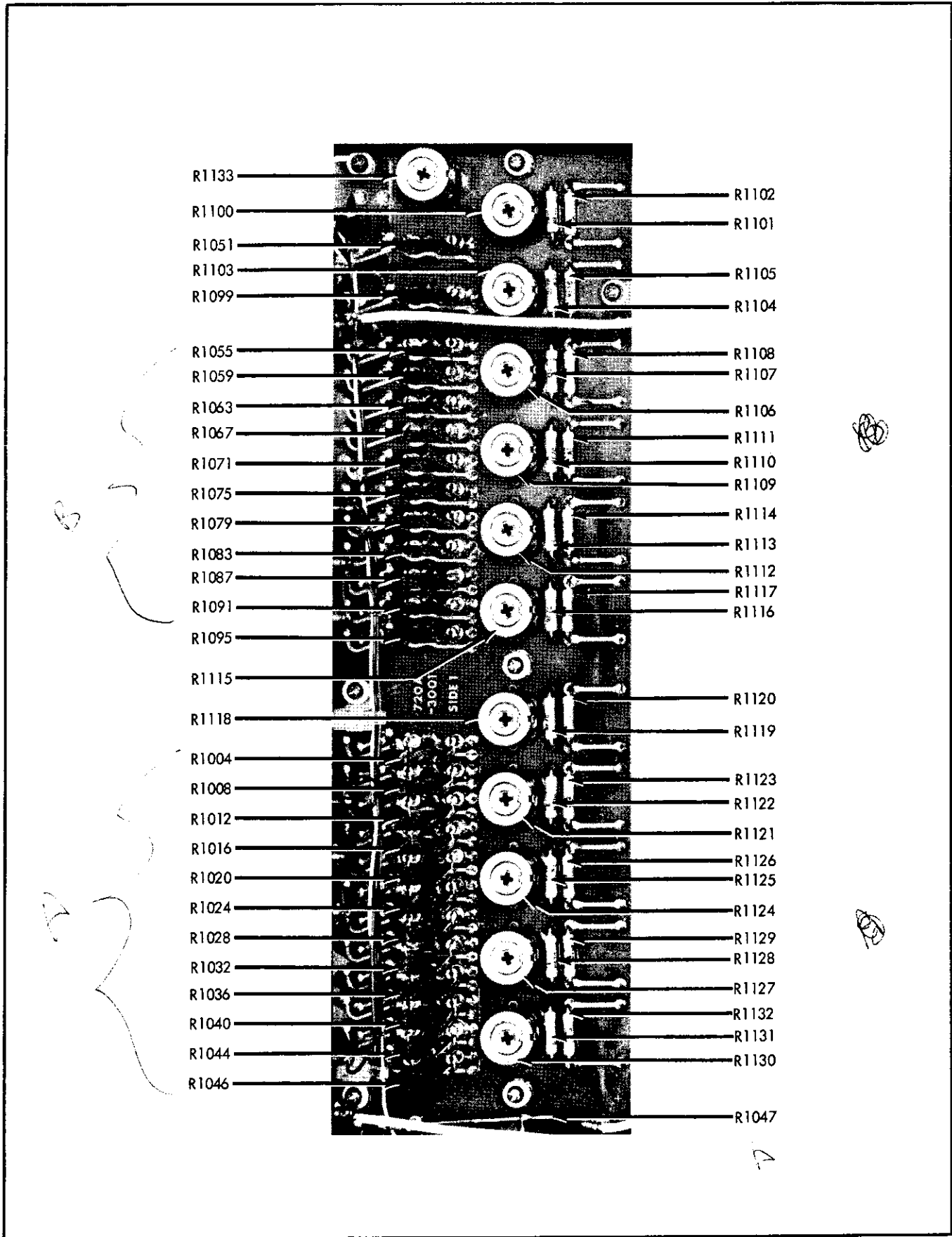


Figure 5-3. TRIMMER P/C ASSEMBLY (Sheet 1 of 2)

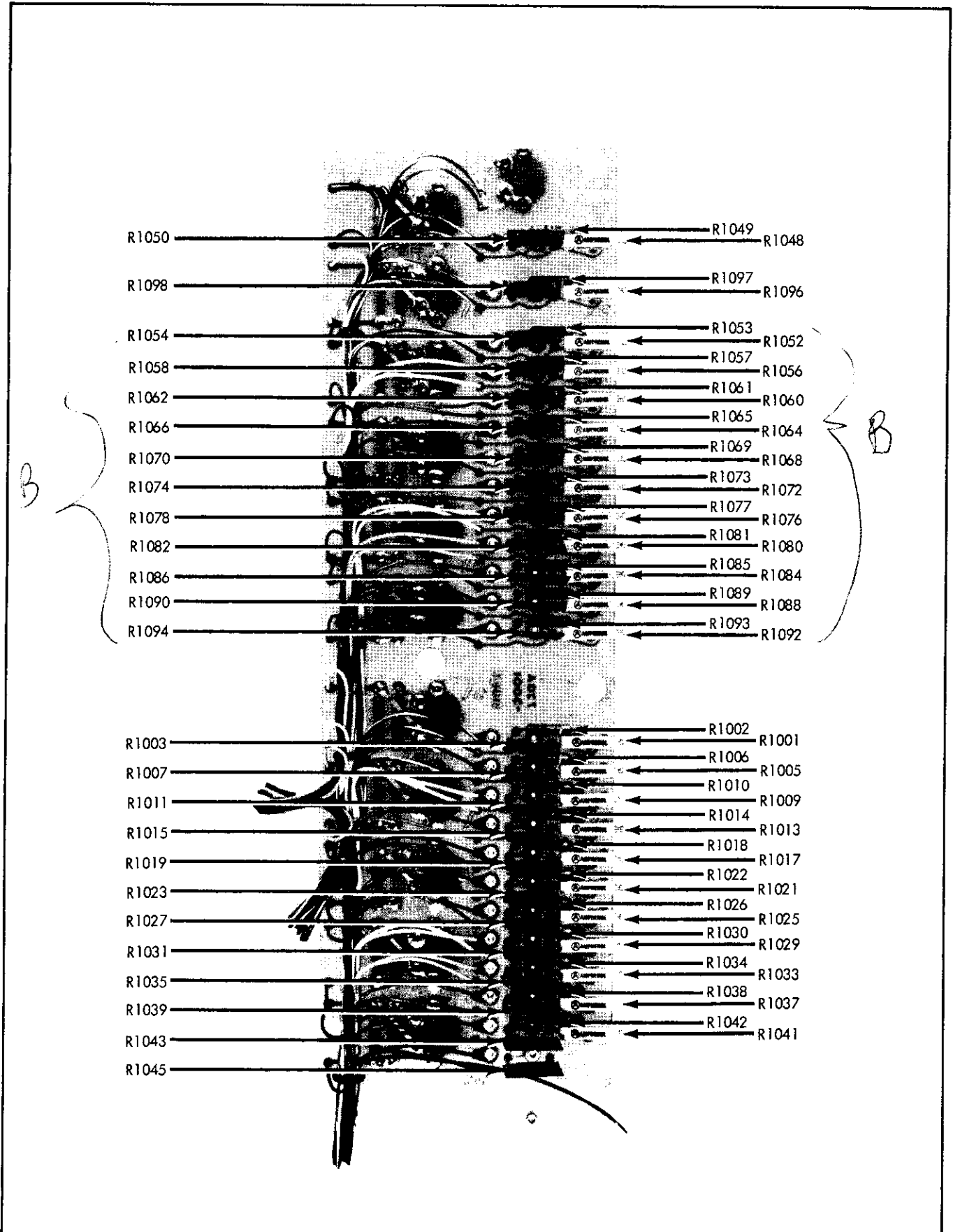







Figure 5-3. TRIMMER P/C ASSEMBLY (Sheet 2 of 2)

REF DESIGN	DESCRIPTION	QTY	UNIT	PRICE	TOTAL	REF QTY	USE CODE
R1049	Res, met flm, 8.45k ±1%, 1/2w	1000	PCB	1000	1000		
R1050	Res, ww, 250Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1051	Res, ww, factory selected	1000	PCB	1000	1000		
R1052	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1053	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1054	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1055	Res, ww, factory selected	1000	PCB	1000	1000		
R1056	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1057	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1058	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1059	Res, ww, factory selected	1000	PCB	1000	1000		
R1060	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1061	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1062	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1063	Res, ww, factory selected	1000	PCB	1000	1000		
R1064	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1065	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1066	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1067	Res, ww, factory selected	1000	PCB	1000	1000		
R1068	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1069	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1070	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1071	Res, ww, factory selected	1000	PCB	1000	1000		
R1072	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1073	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1074	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1075	Res, ww, factory selected	1000	PCB	1000	1000		
R1076	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1077	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1078	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1079	Res, ww, factory selected	1000	PCB	1000	1000		
R1080	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1081	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1082	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1083	Res, ww, factory selected	1000	PCB	1000	1000		
R1084	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1085	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1086	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1087	Res, ww, factory selected	1000	PCB	1000	1000		
R1088	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1089	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1090	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1091	Res, ww, factory selected	1000	PCB	1000	1000		
R1092	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1093	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1094	Res, ww, 100Ω ±0.5%, 1/2w	1000	PCB	1000	1000		
R1095	Res, ww, factory selected	1000	PCB	1000	1000		
R1096	Res, var, ww, 5k ±10%, 1w	1000	PCB	1000	1000		
R1097	Res, met flm, 4.75k ±1%, 1/2w	1000	PCB	1000	1000		
R1098	Res, ww, 400Ω ±0.5%, 1/2w	1000	PCB	1000	1000		

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
R1099	Res, ww, factory selected						
R1100	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	11		
R1101	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	11		
R1102	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	11		
R1103	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1104	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1105	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1106	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1107	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1108	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1109	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1110	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1111	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1112	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1113	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1114	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1115	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1116	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1117	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1118	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1119	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1120	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1121	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1122	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1123	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1124	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1125	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1126	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1127	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1128	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1129	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1130	Res, var, ww, 25Ω ±10%, 1 1/4w	4702-161703	71450	Type 110	REF		
R1131	Res, met flm, 23. 2Ω ±1%, 1/2w	4705-200790	12400	Type CEC-TO	REF		
R1132	Res, met flm, 10Ω ±1%, 1/2w	4705-151043	12400	Type CEC-TO	REF		
R1133	Res, var, ww, 150Ω ±20%, 1 1/4w	4702-163642	71450	Type 110	1		



These resistors are factory selected. Replace with exact value. When ordering, include model, serial number, reference designation and all information stamped on the resistor.

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
	BRIDGE P/C ASSEMBLY - Figure 5-4	1702-200295 (720A-4002)	89536	1702-200295	REF		
R201	Res, ww, 39.536k, matched set						
R202	Res, ww, 39.536k, matched set						
R203	Res, var, ww, 100Ω ±20%, 1 1/4w	4702-112797	71450	Type 110	2		
R204	Res, ww, 15.814k ±0.02%, 1w	4707-200550	89536	4707-200550	1	1	
R205	Res, var, ww, 100Ω ±20%, 1 1/4w	4702-112797	71450	Type 110	REF		
R206	Res, ww, 4.873k, matched set						
R207	Res, ww, 4.873k, matched set						
R208	Res, met flm, 15k ±1%, 1/2w	4705-151498	12400	Type CEC-TO	1		
R209	Res, ww, 250Ω ±0.5%, 1/2w	4707-199893	89536	4707-199893	1	1	



These resistors are factory matched. If replacement is required, an entire set, part number 4710-217679, must be ordered.



These resistors are factory matched. If replacement is required, an entire set, part number 4710-217687, must be ordered.

720A-3002
P/N 200295

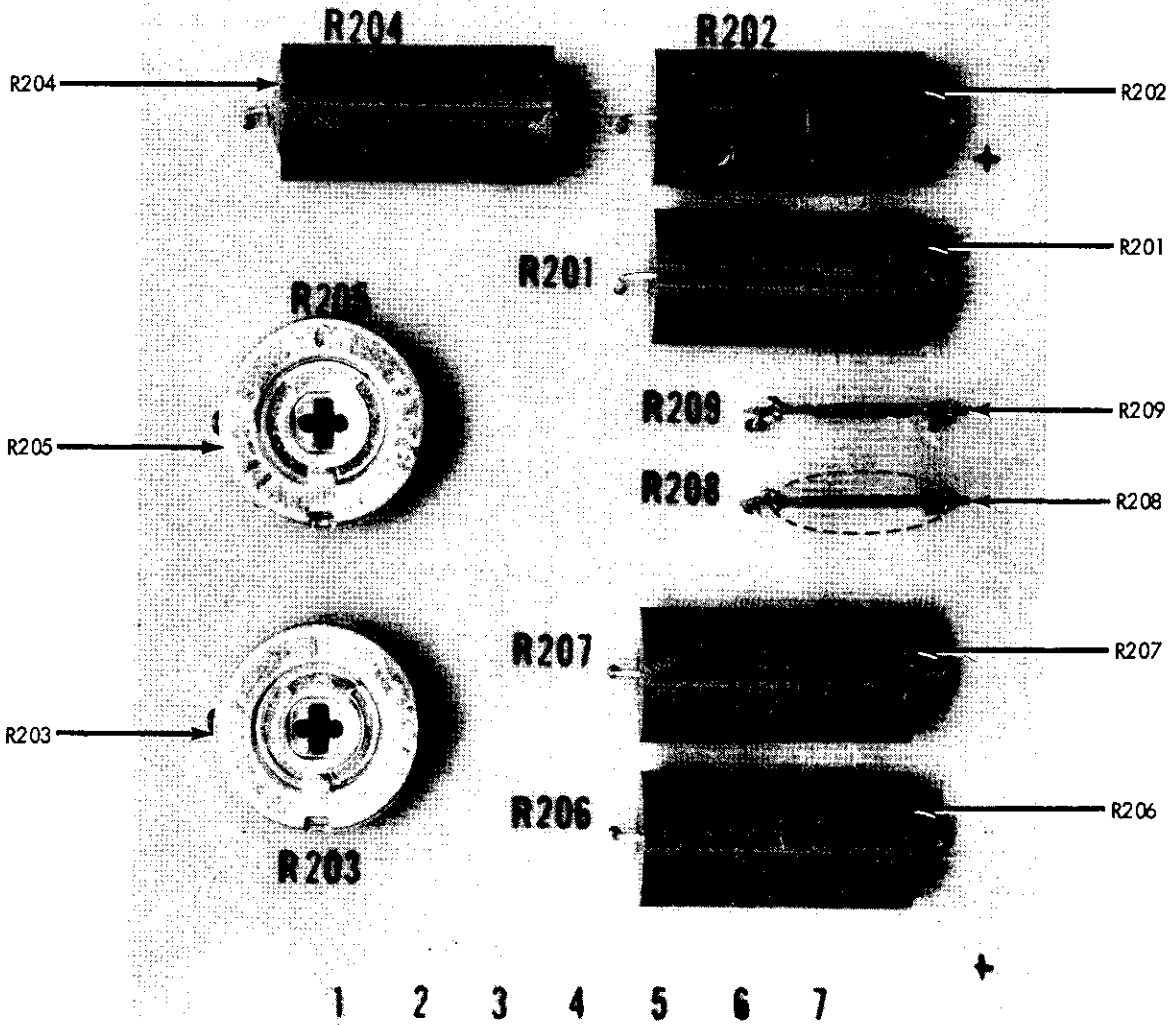
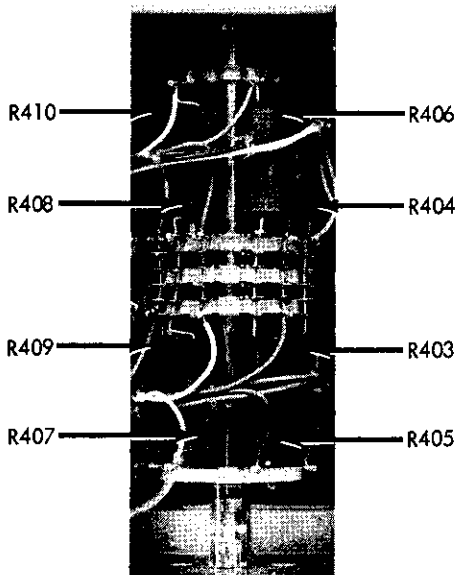


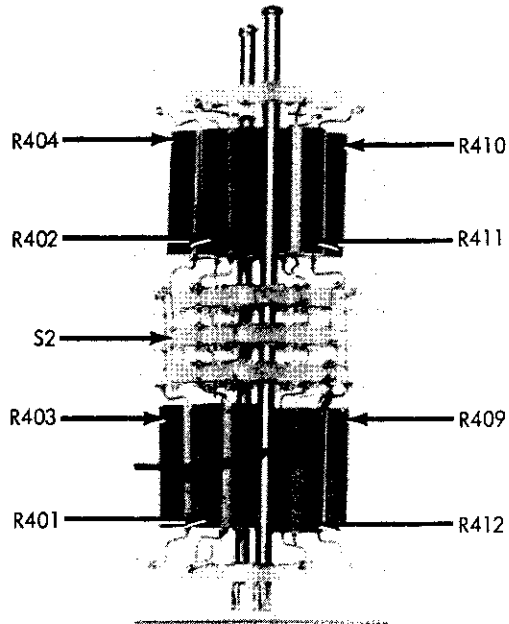
Figure 5-4. BRIDGE P/C ASSEMBLY

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
R401 thru R411	"B" DECADE SWITCH ASSEMBLY Figure 5-5 Res, ww, 9.898k, matched set	5110-217307 (720A-4004)	89536	5110-217307	REF		
R412	Res, ww, 39.536k ±0.01%, 1w	4707-199810	89536	4707-199810	1	1	
S2	Switch, "B", rotary, 3p, 11 pos, 5 sect	5107-218602	89536	5107-218602	2		

△ These resistors are a factory matched set, part number 4710-217646. If replacement of one or more resistors in the set is required, include all information stamped on the resistor along with the information described in paragraph 5-6. Should the information on the resistor not be discernible, include all of the above information about the adjacent resistors.



TOP VIEW



BOTTOM VIEW

Figure 5-5. "B" DECADE SWITCH ASSEMBLY

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
R501 thru R511	"C" DECADE SWITCH ASSEMBLY Figure 5-6 Res, ww, 4k, matched set	5110-217315 (720A-4005)	89536	5110-217315	REF		
R512	Res, ww, 40.31k \pm 0.02%, 1w	4707-199836	89536	4707-199836	1	1	
S3	Switch, "C", rotary, 3p, 11 pos, 5 sect	5107-218602	89536	5107-218602	REF		

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These resistors are a factory matched set, part number 4710-217653. If replacement of one or more resistors in the set is required, include all information stamped on the resistor along with the information described in paragraph 5-6. Should the information on the resistor not be discernible, include all of the above information about the adjacent resistors.

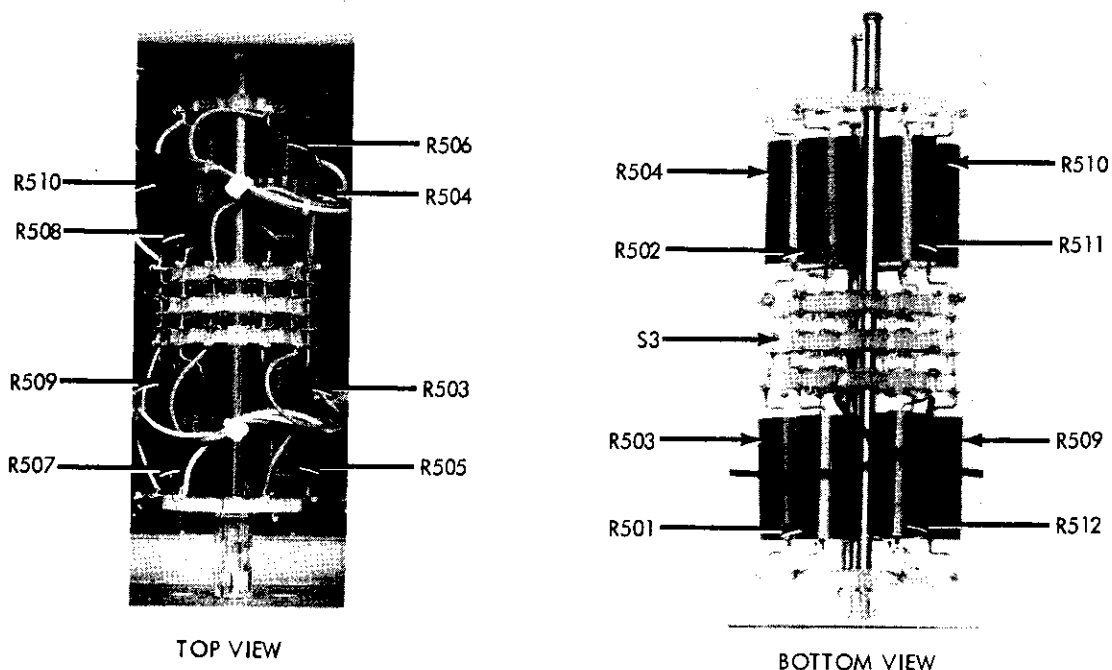









Figure 5-6. "C" DECADE SWITCH ASSEMBLY

REF DESIG	DESCRIPTION	STOCK NO	MFR	MFR PART NO	TOT QTY	REC QTY	USE CODE
	"D", "E", "F", AND "G" DECADES SWITCH ASSEMBLY - Figure 5-7	5110-217323 (720A-4006)	89536	5110-217323	REF		
R601 thru R611	Res, ww, 1k, matched set						
R612	Res, ww, 2.5k, matched set						
R701 thru R711	Res, ww, 1k, matched set						
R712	Res, ww, 2.5k, matched set						
R801 thru R811	Res, ww, 1k, matched set						
R812	Res, ww, 2.5k, matched set						
R901 thru R910	Res, ww, 1k, matched set						
S4	Switch, "D", rotary, 2p, 10 pos, 4 sect	5107-218594	89536	5107-218594	3		
S5	Switch, "E", rotary, 2p, 10 pos, 4 sect	5107-218594	89536	5107-218594	REF		
S6	Switch, "F", rotary, 2p, 10 pos, 4 sect	5107-218594	89536	5107-218594	REF		
S7	Switch, "G", rotary, 1p, 11 pos, 3 sect	5107-218586	89536	5107-218586	1		



These resistors are a factory matched set, part number 4710-217661. If replacement of one or more resistors in the set is required, include all information stamped on the resistor along with the information described in paragraph 5-6. Should the information on the resistor not be discernible, include all of the above information about the adjacent resistors.

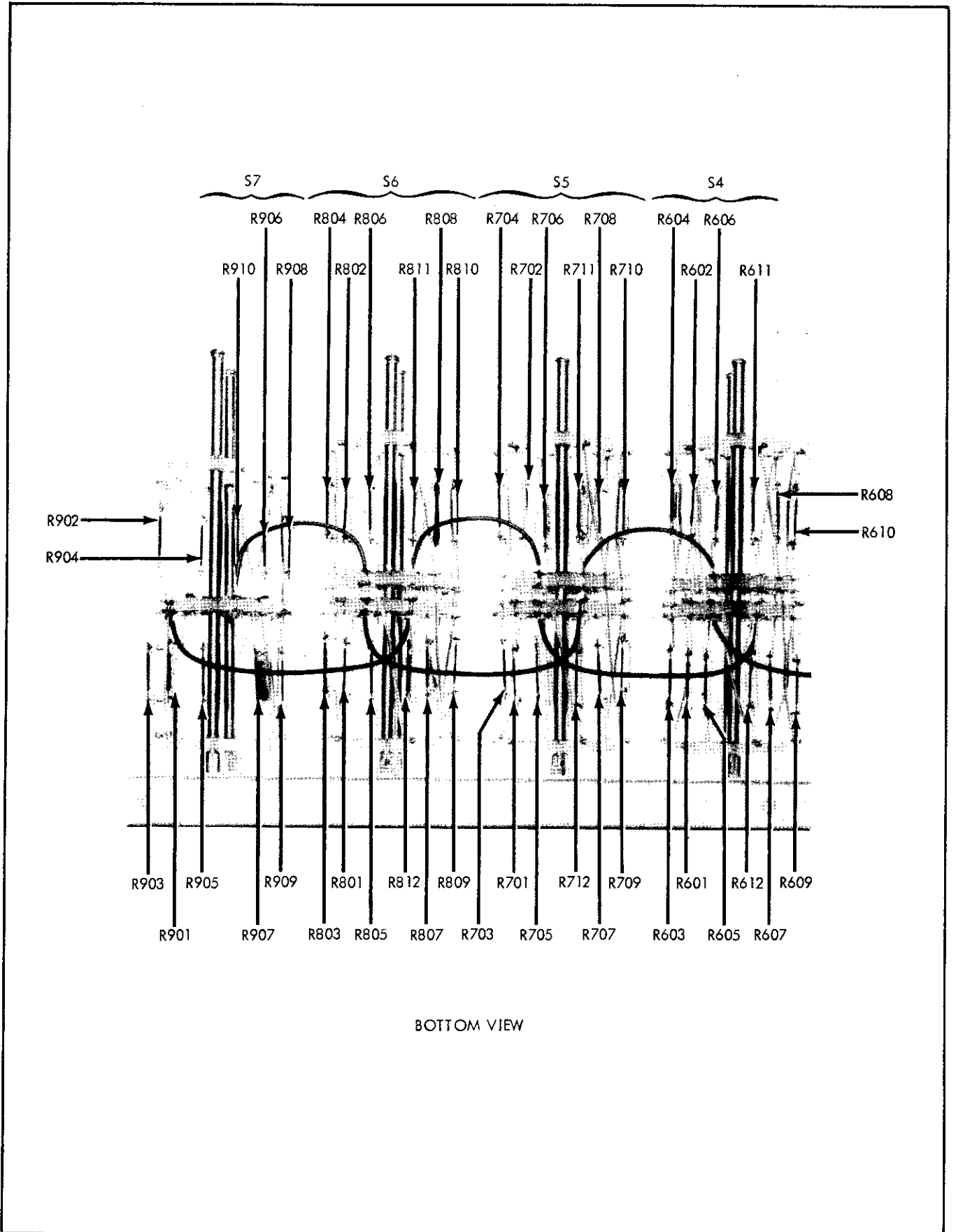


Figure 5-7. "D", "E", "F" AND "G" DECADES SWITCH ASSEMBLY

Section 7

General Information

7-1. This section of the manual contains generalized user information as well as supplemental information to the List of Replaceable Parts contained in Section 5. The following information is presented in this section:

List of Abbreviations

Federal Supply Codes for Manufacturers

Fluke Technical Service Centers — U.S. and Canada

Sales and Service Locations — International

Sales Representatives — U.S. and Canada

List of Abbreviations and Symbols

A or amp	ampere	H	henry	pF	picofarad
ac	alternating current	hd	heavy duty	pn	part number
af	audio frequency	hf	high frequency	(+) or pos	positive
a/d	analog-to-digital	Hz	hertz	pot	potentiometer
assy	assembly	IC	integrated circuit	p-p	peak-to-peak
AWG	american wire gauge	if	intermediate frequency	ppm	parts per million
B	bel	in	inch(es)	PROM	programmable read-only memory
bcd	binary coded decimal	intl	internal	psi	pound-force per square inch
°C	Celsius	I/O	input/output	RAM	random-access memory
cap	capacitor	k	kilo (10 ³)	rf	radio frequency
ccw	counterclockwise	kHz	kilohertz	rms	root mean square
cer	ceramic	kΩ	kilohm(s)	ROM	read-only memory
cermet	ceramic to metal(seal)	kV	kilovolt(s)	s or sec	second (time)
ckt	circuit	lf	low frequency	scope	oscilloscope
cm	centimeter	LED	light-emitting diode	SH	shield
cmrr	common mode rejection ratio	LSB	least significant bit	Si	silicon
comp	composition	LSD	least significant digit	serno	serial number
cont	continue	M	mega (10 ⁶)	sr	shift register
crt	cathode-ray tube	m	milli (10 ⁻³)	Ta	tantalum
cw	clockwise	mA	milliamper(e)s	tb	terminal board
d/a	digital-to-analog	max	maximum	tc	temperature coefficient or temperature compensating
dac	digital-to-analog converter	mf	metal film	tcxo	temperature compensating crystal oscillator
dB	decibel	MHz	megahertz	tp	test point
dc	direct current	min	minimum	u or μ	micro (10 ⁻⁶)
dmm	digital multimeter	mm	millimeter	uhf	ultra high frequency
dvm	digital voltmeter	ms	millisecond	us or μs	microsecond(s) (10 ⁻⁶)
elect	electrolytic	MSB	most significant bit	uut	unit under test
ext	external	MSD	most significant digit	V	volt
F	farad	MTBF	mean time between failures	v	voltage
°F	Fahrenheit	MTTR	mean time to repair	var	variable
FET	Field-effect transistor	mV	millivolt(s)	vco	voltage controlled oscillator
ff	flip-flop	mv	multivibrator	vhf	very high frequency
freq	frequency	MΩ	megohm(s)	vlf	very low frequency
FSN	federal stock number	n	nano (10 ⁻⁹)	W	watt(s)
g	gram	na	not applicable	ww	wire wound
G	giga (10 ⁹)	NC	normally closed	xfmr	transformer
gd	guard	(-) or neg	negative	xstr	transistor
Ge	germanium	NO	normally open	xtal	crystal
GHz	gigahertz	ns	nanosecond	xtlo	crystal oscillator
gmV	guaranteed minimum value	opnl ampl	operational amplifier	Ω	ohm(s)
gnd	ground	p	pico (10 ⁻¹²)	μ	micro (10 ⁻⁶)
		para	paragraph		
		pcb	printed circuit board		

Federal Supply Codes for Manufacturers (Continued)

00213 Nytronics Comp. Group Inc. Subsidiary of Nytronics Inc. Formerly Sage Electronics Rochester, New York	03797 Eidema Div. Genisco Technology Corp. Compton, California	05574 Viking Industries Chatsworth, California	07597 Burndy Corp. Tape/Cable Div. Rochester, New York
00327 Welwyn International, Inc. Westlake, Ohio	03877 Transistron Electronic Corp. Wakefield, Massachusetts	05704 Replaced by 16258	07792 Lerma Engineering Corp. Northampton, Massachusetts
00656 Aerovox Corp. New Bedford, Massachusetts	03888 KDI Pyrofilm Corp. Whippany, New Jersey	05820 Wakefield Engineering Inc. Wakefield, Massachusetts	07910 Teledyne Semiconductor Formerly Continental Device Hawthorne, California
00686 Film Capacitors, Inc. Passaic, New Jersey	03911 Clairex Electronics Div. Clairex Corp. Mt. Vernon, New York	06001 General Electric Co. Electronic Capacitor & Battery Products Dept. Columbia, South Carolina	07933 - use 49956 Raytheon Co. Semiconductor Div. HQ Mountain View, California
00779 AMP Inc. Harrisberg, Pennsylvania	03980 Muirhead Inc. Mountainside, New Jersey	06136 Replaced by 63743	08225 Industro Transistor Corp. Long Island City, New York
01121 Allen-Bradley Co. Milwaukee, Wisconsin	04009 Arrow Hart Inc. Hartford, Connecticut	06383 Panduit Corp. Tinley Park, Illinois	08261 Spectra Strip Corp. Garden Grove, California
01281 TRW Electronic Comp. Semiconductor Operations Lawndale, California	04062 Replaced by 72136	06473 Bunker Ramo Corp. Amphenol SAMS Div. Chatsworth, California	08530 Reliance Mica Corp. Brooklyn, New York
01295 Texas Instruments, Inc. Semiconductor Group Dallas, Texas	04202 Replaced by 81312	06555 Beede Electrical Instrument Co. Penacook, New Hampshire	08806 General Electric Co. Miniature Lamp Products Dept. Cleveland, Ohio
01537 Motorola Communications & Electronics Inc. Franklin Park, Illinois	04217 Essex International Inc. Wire & Cable Div. Anaheim, California	06739 Electron Corp. Littleton, Colorado	08863 Nylomatic Corp. Norrisville, Pennsylvania
01686 RCL Electronics Inc. Manchester, New Hampshire	04221 Aemco, Div. of Midtex Inc. Mankato, Minnesota	06743 Clevite Corp. Cleveland, Ohio	08988 - use 53085 Skottie Electronics Inc. Archbald, Pennsylvania
01730 Replaced by 73586	04222 AVX Ceramics Div. AVX Corp. Myrtle Beach, Florida	06751 Components, Inc. Semicor Div. Phoenix, Arizona	09214 G.E. Co. Semi-Conductor Products Dept. Power Semi-Conductor Products OPN Sec. Auburn, New York
01884 - use 56289 Sprague Electric Co. Dearborn Electronic Div. Lockwood, Florida	04423 Telonic Industries Laguna Beach, California	06860 Gould Automotive Div. City of Industry, California	09353 C and K Components Watertown, Massachusetts
02114 Ferroxcube Corp. Saugerties, New York	04645 Replaced by 75376	06961 Vernitron Corp., Piezo Electric Div. Formerly Clevite Corp., Piezo Electric Div. Bedford, Ohio	09423 Scientific Components, Inc. Santa Barbara, California
02131 General Instrument Corp. Harris ASW Div. Westwood, Maine	04713 Motorola Inc. Semiconductor Products Phoenix, Arizona	06980 Eimac Div. Varian Associates San Carlos, California	09922 Burndy Corp. Norwalk, Connecticut
02395 Rason Mfg. Co. Brooklyn, New York	04946 Standard Wire & Cable Los Angeles, California	07047 Ross Milton, Co., The South Hampton, Pennsylvania	09969 Dale Electronics Inc. Yankton, S. Dakota
02533 Snelgrove, C.R. Co., Ltd. Don Mills, Ontario, Canada M3B 1M2	05082 Replaced by 94988	07115 Replaced by 14674	10059 Barker Engineering Corp. Formerly Amerace, Amerace ESNA Corp. Kenilworth, New Jersey
02606 Fenwal Labs Div. of Travenal Labs. Morton Grove, Illinois	05236 Jonathan Mfg. Co. Fullerton, California	07138 Westinghouse Electric Corp., Electronic Tube Division Horsehead, New York	11236 CTS of Berne Berne, Indiana
02660 Bunker Ramo Corp., Conn Div. Formerly Amphenol-Borg Electric Corp. Broadview, Illinois	05245 Components Corp. now Corcom, Inc. Chicago, Illinois	07233 TRW Electronic Components Cinch Graphic City of Industry, California	11237 CTS Keene Inc. Paso Robles, California
02799 Aero Capacitors, Inc. Chatsworth, California	05277 Westinghouse Electric Corp. Semiconductor Div. Youngwood, Pennsylvania	07256 Silicon Transistor Corp. Div. of BBF Group Inc. Chelmsford, MA	11358 CBS Electronic Div. Columbia Broadcasting System Newburyport, MN
03508 General Electric Co. Semiconductor Products Syracuse, New York	05278 Replaced by 43543	07261 Aumet Corp. Culver City, California	11403 Best Products Co. Chicago, Illinois
03614 Replaced by 71400	05279 Southwest Machine & Plastic Co. Glendora, California	07263 Fairchild Semiconductor Div. of Fairchild Camera & Instrument Corp. Mountain View, California	11503 Keystone Columbia Inc. Warren, Michigan
03651 Replaced by 44655	05397 Union Carbide Corp. Materials Systems Div. New York, New York	07344 Bircher Co., Inc. Rochester, New York	11532 Teledyne Relays Hawthorne, California
	05571 - use 56289 Sprague Electric Co. Pacific Div. Los Angeles, California		

Federal Supply Codes for Manufacturers (Continued)

11711 General Instrument Corp Rectifier Division Hickville, New York	14099 Semtech Corp. Newbury Park, California	17069 Circuit Structures Lab. Burbank, California	24655 General Radio Concord, Massachusetts
11726 Qualidyne Corp. Santa Clara, California	14140 Edison Electronic Div. Mc Gray-Edison Co. Manchester, New Hampshire	17338 High Pressure Eng. Co., Inc. Oklahoma City, Oklahoma	24759 Lenox-Fugle Electronics Inc. South Plainfield, New Jersey
12014 Chicago Rivet & Machine Co. Bellwood, Illinois	14193 Cal-R-Inc. formerly California Resistor, Corp. Santa Monica, California	17545 Atlantic Semiconductors, Inc. Asbury Park, New Jersey	25088 Siemen Corp. Isilen, New Jersey
12040 National Semiconductor Corp. Danbury, Connecticut	14298 American Components, Inc. an Insilco Co. Conshohocken, Pennsylvania	17856 Siliconix, Inc. Santa Clara, California	25403 Amperex Electronic Corp. Semiconductor & Micro-Circuits Div. Slatersville, Rhode Island
12060 Diodes, Inc. Chatsworth, California	14655 Cornell-Dublier Electronics Division of Federal Pacific Electric Co. Govt. Control Dept. Newark, New Jersey	17870 Replaced by 14140	27014 National Semiconductor Corp. Santa Clara, California
12136 Philadelphia Handle Co. Camden, New Jersey	14752 Electro Cube Inc. San Gabriel, California	18178 Vactec Inc. Maryland Heights, Missouri	27264 Molex Products Downers Grove, Illinois
12300 Potter-Brumfield Division AMF Canada LTD. Guelph, Onatrio, Canada	14869 Replaced by 96853	18324 Signetics Corp. Sunnyvale, California	28213 Minnesota Mining & Mfg. Co. Consumer Products Div. St. Paul, Minnesota
12323 Presin Co., Inc. Shelton, Connecticut	14936 General Instrument Corp. Semi Conductor Products Group Hicksville, New York	18612 Vishay Resistor Products Div. Vishay Intertechnology Inc. Malvern, Pennsylvania	28425 Serv-/Link formerly Bohannon Industries Fort Worth, Texas
12327 Freeway Corp. formerly Freeway Washer & Stamping Co. Cleveland, Ohio	15636 Elec-Trol Inc. Saugus, California	18736 Voltronics Corp. Hanover, New Jersey	28478 Deltrol Controls Div. Deltrol Corporation Milwaukee, Wisconsin
12443 Budd Co. The, Polychem Products Plastic Products Div. Bridgeport, PA	15801 Fenwal Electronics Inc. Div. of Kidde Walter and Co., Inc. Framingham, Massachusetts	18927 G T E Sylvania Inc. Precision Material Group Parts Division Titusville, Pennsylvania	28480 Hewlett Packard Co. Corporate H.Q. Palo Alto, California
12615 U.S. Terminals Inc. Cincinnati, Ohio	15818 Teledyne Semiconductors, formerly Amelco Semiconductor Mountain View, California	19451 Perine Machinery & Supply Co. Seattle, Washington	28520 Heyman Mfg. Co. Kenilworth, New Jersey
12617 Hamlin Inc. Lake Mills, Wisconsin	15849 Litton Systems Inc. Useco Div. formerly Useco inc. Van Nuys, California	19701 Electro-Midland Corp. Mecco-Electra Inc. Mineral Wells, Texas	29083 Monsanto, Co., Inc. Santa Clara, California
12697 Clarostat Mfg. Co. Dover, New Hampshire	15898 International Business Machines Corp. Essex Junction, Vermont	20584 Enochs Mfg. Inc. Indianapolis, Indiana	29604 Stackpole Components Co. Raleigh, North Carolina
12749 James Electronics Chicago, Illinois	16258 Space-Lok Inc. Burbank, California	20891 Self-Organizing Systems, Inc. Dallas, Texas	30148 A B Enterprise Inc. Ahoskie, North Carolina
12856 Micrometals Sierra Madre, California	16299 Corning Glass Electronic Components Div. Raleigh, North Carolina	21604 Buckeye Stamping Co. Columbus, Ohio	30323 Illinois Tool Works, Inc. Chicago, Illinois
12954 Dickson Electronics Corp. Scottsdale, Arizona	16332 Replaced by 14140	21845 Solitron Devices Inc. Transistor Division Riveria Beach, Florida	31091 Optimax Inc. Colimar, Pennsylvania
12969 Unitrode Corp. Watertown, Massachusetts	16473 Cambridge Scientific Ind. Div. of Chemed Corporation Cambridge, Maryland	22767 ITT Semiconductors Palo Alto, California	32539 Mura Corp. Great Neck, New York
13103 Thermalloy Co., Inc. Dallas, Texas	16742 Paramount Plastics Fabricators, Inc. Downey, California	23050 Product Comp. Corp. Mount Vernon, New York	32767 Griffith Plastic Corp. Burlingame, California
13327 Solitron Devices Inc. Tappan, New York	16758 Delco Electronics Div. of General Motors Corp. Kokomo, Indiana	23732 Tracor Inc. Rockville, Maryland	32879 Advanced Mechanical Components Northridge, California
13511 Amphenol Cadre Div. Bunker-Ramo Corp. Los Gatos, California	17001 Replaced by 71468	23880 Stanford Applied Engrng. Santa Clara, California	32897 Erie Technological Products, Inc. Frequency Control Div. Carlisle, Pennsylvania
13606 - use 56289 Sprague Electric Co. Transistor Div. Concord, New Hampshire		23936 Pamotor Div., Wm. J. Purdy Co. Burlingame, California	32997 Bourns Inc. Trimpot Products Division Riverside, California
13839 Replaced by 23732		24248 Replaced by 94222	33173 General Electric Co. Products Dept. Owensboro, Kentucky
		24355 Analog Devices Inc. Norwood, Massachusetts	

Federal Supply Codes for Manufacturers (Continued)

34333 Silicon General Westminister, California	70563 Amperite Company Union City, New Jersey	73293 Hughes Aircraft Co. Electron Dynamics Div. Torrence, California	77969 Rubbercraft Corp. of CA. LTD. Torrance, California
34335 Advanced Micro Devices Sunnyvale, California	70903 Belden Corp. Geneva, Illinois	73445 Amperex Electronic Corp. Hicksville, LI, New York	78189 Shakeproof Div. of Illinois Tool Works Inc. Elgin, Illinois
34802 Electromotive Inc. Kenilworth, New Jersey	71002 Birnbach Radio Co., Inc. Freeport, LI New York	73559 Carling Electric Inc. West Hartford, Connecticut	78277 Sigma Instruments, Inc. South Braintree, Massachusetts
37942 Mallory, P.R. & Co., Inc. Indianapolis, Indiana	71400 Bussmann Mfg. Div. of McGraw-Edison Co. Saint Louis, Missouri	73586 Circle F Industries Trenton, New Jersey	78488 Stackpole Carbon Co. Saint Marys, Pennsylvania
42498 National Radio Melrose, Massachusetts	71450 CTS Corp. Elkhart, Indiana	73734 Federal Screw Products, Inc. Chicago, Illinois	78553 Eaton Corp. Engineered Fastener Div. Tinnerman Plant Cleveland, Ohio
43543 Nytronics Inc. Transformer Co. Div. Geneva, New York	71468 ITT Cannon Electric Inc. Santa Ana, California	73743 Fischer Special Mfg. Co. Cincinnati, Ohio	79136 Waldes Kohinoor Inc. Long Island City, New York
44655 Ohmite Mfg. Co. Skokie, Illinois	71482 Clare, C.P. & Co. Chicago, Illinois	73899 JFD Electronics Co. Components Corp Brooklyn, New York	79497 Western Rubber Company Goshen, Indiana
49671 RCA Corp. New York, New York	71590 Centrelab Electronics Div. of Globe Union Inc. Milwaukee, Wisconsin	73949 Guardian Electric Mfg. Co. Chicago, Illinois	79963 Zierick Mfg. Corp. Mt. Kisko, New York
49956 Raytheon Company Lexington, Massachusetts	71707 Coto Coil Co., Inc. Providence, Rhode Island	74199 Quan Nichols Co. Chicago, Illinois	80031 Electro-Midland Corp., Mepco Div. A North American Phillips Co. Morristown, New Jersey
50088 Mostek Corp. Carrollton, Texas	71744 Chicago Miniature Lamp Works Chicago, Illinois	74217 Radio Switch Corp. Marlboro, New Jersey	80145 LFE Corp., Process Control Div. formerly API Instrument Co. Chesterland, Ohio
50579 Litronix Inc. Cupertino, California	71785 TRW Electronics Components Cinch Connector Operations Div. Elk Grove Village, Chicago, Illinois	74276 Signalite Div. General Instrument Corp. Neptune, New Jersey	80183 - use 56289 Sprague Products North Adams, Massachusetts
51605 Scientific Components Inc. Linden, New Jersey	72005 Driver, Wilber B., Co. Newark, New Jersey	74306 Piezo Crystal Co. Carlisle, Pennsylvania	80294 Bourns Inc., Instrument Div. Riverside, California
53021 Sangamo Electric Co. Springfield, Illinois	72092 Replaced by 06980	74542 Hoyt Elect. Instr. Works Penacook, New Hampshire	80583 Hammarlund Mfg. Co., Inc. Red Bank, New Jersey
54294 Cutler-Hammer Inc. formerly Shallcross, A Cutter-Hammer Co. Selma, North Carolina	72136 Electro Motive Mfg. Co. Williamantic, Connecticut	74970 Johnson E.F., Co. Waseca, Minnesota	80640 Stevens, Arnold Inc. South Boston, Massachusetts
55026 Simpson Electric Co. Div. of Am. Gage and Mach. Co. Elgin, Illinois	72259 Nytronics Inc. Pelham Manor, New Jersey	75042 TRW Electronics Components IRC Fixed Resistors Philadelphia, Pennsylvania	81073 Grayhill, Inc. La Grange, Illinois
56289 Sprague Electric Co. North Adams, Massachusetts	72619 Dialight Div. Amperex Electronic Corp. Brooklyn, New York	75376 Kurz-Kasch Inc. Dayton, Ohio	81312 Winchester Electronics Div. of Litton Industries Inc. Oakville, Connecticut
58474 Superior Electric Co. Bristol, Connecticut	72653 G.C. Electronics Div. of Hydrometals, Inc. Brooklyn, New York	75378 CTS Knights Inc. Sandwich, Illinois	81439 Therm-O-Disc Inc. Mansfield, Ohio
60399 Torin Corp. formerly Torrington Mfg. Co. Torrington, Connecticut	72665 Replaced by 90303	75382 Kulka Electric Corp. Mount Vernon, New York	81483 International Rectifier Corp. Los Angeles, California
63743 Ward Leonard Electric Co., Inc. Mount Vernon, New York	72794 Dzus Fastener Co., Inc. West Islip, New York	75915 Littlefuse Inc. Des Plaines, Illinois	81590 Korry Mfg. Co. Seattle, Washington
64834 West Mfg. Co. San Francisco, California	72928 Gulton Ind. Inc. Gudeman Div. Chicago, Illinois	76854 Oak Industries Inc. Switch Div. Crystal Lake, Illinois	81741 Chicago Lock Co. Chicago, Illinois
65092 Weston Instruments Inc. Newark, New Jersey	72982 Erie Tech. Products Inc. Erie, Pennsylvania	77342 AMF Inc. Potter & Brumfield Div. Princeton, Indiana	82305 Palmer Electronics Corp. South Gate, California
66150 Winslow Tele-Tronics Inc. Eaton Town, New Jersey	73138 Beckman Instruments Inc. Helipot Division Fullerton, California	77638 General Instrument Corp. Rectifier Division Brooklyn, New York	82389 Switchcraft Inc. Chicago, Illinois
70485 Atlantic India Rubber Works Chicago, Illinois			

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82415 North American Phillips Controls Corp. Frederick, Maryland	88245 Litton Systems Inc. Useco Div. Van Nuys, California	91934 Miller Electric Co., Inc. Div of Aunet Woonsocket, Rhode Island	97966 Replaced by 11358
82872 Roanwell Corp. New York, New York	88419 Cornell-Dubilier Electronic Div. Federal Pacific Co. Fuquay-Varian, North Carolina	92194 Alpha Wire Corp. Elizabeth, New Jersey	98094 Replaced by 49956
82877 Rotron Inc. Woodstock, New York	88486 Plastic Wire & Cable Jewitt City, Connecticut	93332 Sylvania Electric Products Semiconductor Products Div. Woburn, Massachusetts	98159 Rubber-Teck, Inc. Gardena, California
82879 ITT Royal Electric Div. Pawtucket, Rhode Island	88690 Replaced by 04217	94145 Replaced by 49956	98278 Malco A Microdot Co., Inc. Connector & Cable Div. Pasadena, California
83003 Varo Inc. Garland, Texas	89536 Fluke, John Mfg. Co., Inc. Seattle, Washington	94154 - use 94988 Wagner Electric Corp. Tung-Sol Div. Newark, New Jersey	98291 Sealectro Corp. Mamaroneck, New York
83058 Carr Co., The United Can Div. of TRW Cambridge, Massachusetts	89730 G.E. Co., Newark Lamp Works Newark, New Jersey	94222 Southco Inc. formerly South Chester Corp. Lester, Pennsylvania	98388 Royal Industries Products Div. San Diego, California
83298 Bendix Corp. Electric Power Division Eatontown, New Jersey	90201 Mallory Capacitor Co. Div of P.R. Mallory Co., Inc. Indianapolis, Indiana	95146 Alco Electronic Products Inc. Lawrence, Massachusetts	98743 Replaced by 12749
83330 Smith, Herman H., Inc. Brooklyn, New York	90211 - use 56365 Square D Co. Chicago, Illinois	95263 Leecraft Mfg. Co. Long Island City, New York	98925 Replaced by 14433
83478 Rubbercraft Corp. of America, Inc. West Haven, Connecticut	90215 Best Stamp & Mfg. Co. Kansas City, Missouri	95264 Replaced by 98278	99120 Plastic Capacitors, Inc. Chicago, Illinois
83594 Burroughs Corp. Electronic Components Div. Plainfield, New Jersey	90303 Mallory Battery Co. Div. of Mallory Co., Inc. Tarrytown, New York	95275 Vitramon Inc. Bridgeport, Connecticut	99217 Bell Industries Elect. Comp. Div. formerly Southern Elect. Div. Burbank, California
83740 Union Carbide Corp. Battery Products Div. formerly Consumer Products Div. New York, New York	91094 Essex International Inc. Suglex/IWP Div. Newmarket, New Hampshire	95303 RCA Corp. Receiving Tube Div. Cincinnati, Ohio	99392 STM Oakland, California
84171 Arco Electronics Great Neck, New York	91293 Johanson Mfg. Co. Boonton, New Jersey	95348 Gordo's Corp. Bloomfield, New Jersey	99515 ITT Jennings Monrovia Plant Div. of ITT Jennings formerly Marshall Industries Capacitor Div. Monrovia, California
84411 TRW Electronic Components TRW Capacitors Ogallala, Nebraska	91407 Replaced by 58474	95354 Methode Mfg. Corp. Rolling Meadows, Illinois	99779 - use 29587 Bunker-Ramo Corp. Barnes Div. Landsdowne, Pennsylvania
84613 Fuse Indicator Corp. Rockville, Maryland	91502 Associated Machine Santa Clara, California	95712 Bendix Corp. Electrical Components Div. Microwave Devices Plant Franklin, Indiana	99800 American Precision Industries Inc. Delevan Division East Aurora, New York
84682 Essex International Inc. Industrial Wire Div. Peabody, Massachusetts	91506 Augat Inc. Attleboro, Massachusetts	95987 Wackesser Co. Inc. Chicago, Illinois	99942 Centrelab Semiconductor Centrelab Electronics Div. of Globe-Union Inc. El Monte, California
86577 Precision Metal Products, of Malden Inc. Stoneham, Massachusetts	91637 Date Electronics Inc. Columbus, Nebraska	96733 San Fernando Electric Mfg. Co. San Fernando, California	Toyo Electronics (R-Ohm Corp.) Irvine, California
86684 Radio Corp. of America Electronic Components Div. Harrison, New Jersey	91662 Elco Corp. Willow Grove, Pennsylvania	96853 Gulton Industries Inc. Measurement and Controls Div. formerly Rustrak Instruments Co. Manchester, New Hampshire	National Connector Minneapolis, Minnesota
86928 Seastrom Mfg. Co., Inc. Glendale, California	91737 - use 71468 Gremar Mfg. Co., Inc. ITT Cannon/Gremar Santa Ana, California	96881 Thomson Industries, Inc. Manhasset, New York	
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88219 Gould Inc. Industrial Div. Trenton, New Jersey	91833 Keystone Electronics Corp. New York, New York	97913 Industrial Electronic Hdware Corp. New York, New York	
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